

Steady State Thermodynamics

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Received June 3, 2005; accepted November 22, 2005

Published Online: August 11, 2006

The present paper reports our attempt to search for a new universal framework in nonequilibrium physics. We propose a thermodynamic formalism that is expected to apply to a large class of nonequilibrium steady states including a heat conducting fluid, a sheared fluid, and an electrically conducting fluid. We call our theory steady state thermodynamics (SST) after Oono and Paniconi's original proposal. The construction of SST is based on a careful examination of how the basic notions in thermodynamics should be modified in nonequilibrium steady states. We define all thermodynamic quantities through operational procedures which can be (in principle) realized experimentally. Based on SST thus constructed, we make some nontrivial predictions, including an extension of Einstein's formula on density fluctuation, an extension of the minimum work principle, the existence of a new osmotic pressure of a purely nonequilibrium origin, and a shift of coexistence temperature. All these predictions may be checked experimentally to test SST for its quantitative validity.

KEY WORDS: nonequilibrium steady state, thermodynamics, fluctuation

CONTENTS

1 INTRODUCTION	128
1.1 Motivation and the Goal of the Paper	128
1.2 A Quick Look at Steady State Thermodynamics (SST)	131
1.2.1 Nonequilibrium Steady State in a Sheared Fluid	131
1.2.2 Pressure and Chemical Potential	132
1.2.3 Helmholtz Free Energy	133
1.2.4 Flux-Induced Osmosis and Shift of Coexistence Temperature	134

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1.3	Existing Approaches to Nonequilibrium	
	Steady States	136
1.3.1	Phenomenological Theories in the Linear	
	Nonequilibrium Regime	136
1.3.2	Approaches from Microscopic Dynamics	138
1.3.3	Approaches from Meso-Scale Models	140
1.3.4	Recent Progress	141
1.3.5	Thermodynamics Beyond Local Equilibrium Hypothesis	143
2	BRIEF REVIEW OF EQUILIBRIUM PHYSICS	145
2.1	Equilibrium Thermodynamics	145
2.1.1	Equilibrium States and Operations	145
2.1.2	Helmholtz Free Energy	146
2.1.3	Variational Principles and Other Quantities	147
2.2	Statistical Mechanics	149
2.3	Markov Processes	150
2.3.1	Definition of a General Markov Process	151
2.3.2	Detailed Balance Condition	151
2.3.3	The Second Law	152
3	NOEQUILIBRIUM STEADY STATES	
	AND LOCAL STEADY STATES	154
3.1	Nonequilibrium Steady States	154
3.1.1	Heat Conduction	154
3.1.2	Shear Flow	155
3.1.3	Electrical Conduction in a Fluid	156
3.2	Local Steady State	157
3.3	Realization of Local Steady States	157
3.3.1	Heat Conduction	157
3.3.2	Shear Flow	159
3.3.3	Electrical Conduction in a Fluid	159
4	BASIC FRAMEWORK OF STEADY STATE	
	THERMODYNAMICS	159
4.1	Operations to Local Steady States	159
4.2	Choice of Nonequilibrium Variables	162
4.3	Shear Flow	165
4.4	Electrical Conduction in a Fluid	166
5	OPERATIONAL DETERMINATION	
	OF THERMODYNAMIC QUANTITIES	167
5.1	Pressure-A Mechanical Definition	168
5.2	Potential Variation Method and Chemical Potential	169

Steady State Thermodynamics	127
5.3 Maxwell Relation	170
6 SST FREE ENERGY AND ITS POSSIBLE ROLES	171
6.1 Definition of Free Energy	171
6.2 Density Fluctuation	172
6.3 Minimum Work Principle	174
7 STEADY STATE THERMODYNAMICS (SST)	
IN A COMPLETE FORM	175
7.1 Contact of a Steady State and an Equilibrium State	175
7.2 Complete Determination of the Chemical Potential	177
7.3 Complete Determination of the Free Energy	177
7.4 Flux Induced Osmosis (FIO)	179
7.5 μ -Wall Revisited	180
7.6 Shift of Coexistence Temperature	181
8 DISCUSSIONS	183
8.1 Summary and Perspective	183
8.2 Possibility of Experimental Tests	184
8.2.1 Chemical Potential and Fluctuation	184
8.2.2 Flux Induced Osmosis	186
8.3 Frequently Asked Questions	188
8.3.1 What is “Temperature” in Nonequilibrium Steady States?	188
8.3.2 Don’t Long-Range Correlations Destroy Thermodynamics?	189
8.3.3 Why do you Consider Walls and Contacts?	190
8.3.4 Is SST Useful?	190
APPENDIX A: WEAK CONTACT, DENSITY FLUCTUATION, AND LINEAR RESPONSE IN A SHEARED FLUID	191
A.1 Weak Contact Scheme	191
A.2 Balance Condition and the Chemical Potential	193
A.3 Density Fluctuation	194
A.4 Linear Transport	195
A.5 Discussion	198
APPENDIX B: SST IN THE DRIVEN LATTICE GAS	198
B.1 Definition	199
B.2 Local Detailed Balance Condition	202
B.3 Determination of Thermodynamic Quantities	202
B.3.1 Weak contact in Lattice Gases	202
B.3.2 Chemical Potential of Lattice Gases	206
B.3.3 Pressure of Lattice Gases	207
B.3.4 Free Energy of Lattice Gases	208

B.4	Steady State and Density Fluctuation	209
B.5	Minimum Work Principle	210
B.6	Linear Response	213
B.7	μ -Wall in the Driven Lattice Gas	216
B.8	Perturbative Estimate of the SST Free Energy	217
C	THE “SECOND LAW” FOR A GENERAL TIME-DEPENDENT MARKOV PROCESS	221
C.1	Main Results	221
C.2	Proof	221
	ACKNOWLEDGMENTS	223
	REFERENCES	223

1. INTRODUCTION

1.1. Motivation and the Goal of the Paper

Construction of statistical mechanics that applies to nonequilibrium states has been a challenging open problem in theoretical physics. By statistical mechanics, we mean a universal theoretical framework that enables one to precisely characterize states of a given system, and to compute (in principle) arbitrary macroscopic quantities. Nobody knows what the desired nonequilibrium statistical mechanics should look like. Indeed it seems highly unlikely that there is statistical mechanics that applies to *any* nonequilibrium systems. A much more modest (but still extremely ambitious) goal is to look for a theory that applies to nonequilibrium steady states, which are out of equilibrium but have no macroscopically observable time dependence. There may be a chance that probability distributions for nonequilibrium steady states can be obtained from a general principle, analogous to the equilibrium statistical mechanics. Our ultimate goal is to find such a principle, but the goal (if any) is still very far away.

We wish to recall the history of equilibrium statistical mechanics. When Boltzmann, Gibbs, and others constructed statistical mechanics, the formalism of thermodynamics played a fundamental role as a theoretical guide. In particular, Gibbs seems to have intentionally sought for a probability distribution which most naturally recovers some of the thermodynamic relations.

In our attempt toward nonequilibrium statistical mechanics, we too would like to start from the level of phenomenology and look for a possible thermodynamics. By a thermodynamics, we mean a rigid mathematical structure consisting of mathematical relations among certain quantities in a physical system. The mathematical structure of thermodynamics is clearly and abstractly explained, for example, in Refs. 1–3. The conventional thermodynamics for equilibrium systems is a typical

and no doubt the most important example of thermodynamics, but it is not the only example (see, for example, Sec. 3 of Ref. 2 and Appendix A1 of Ref. 4).

Then it makes sense to look for a thermodynamics in a physical context other than equilibrium systems. We wish to do that for nonequilibrium steady states. If it turns out that there is no sensible thermodynamics for nonequilibrium steady states, then we should give up seeking for statistical mechanics. If there is a thermodynamics, on the other hand, then we can start looking for statistical mechanics which is consistent with the thermodynamics. Our goal in the present paper is to propose a thermodynamics for nonequilibrium steady states, and to convince the readers that our proposal is essentially the unique possible thermodynamics.

The standard theory of nonequilibrium thermodynamics (see Sec. 1.3.1) is based on the local equilibrium hypothesis, which roughly asserts that each small part of a nonequilibrium state can be regarded as a copy of a suitable equilibrium state. But such a description seems insufficient for general nonequilibrium steady states, especially when the “degree of nonequilibrium” is not small.

Consider, for example, a system with steady heat flow. It is true that quantities like the temperature and the density become essentially constant within a sufficiently small portion of the system. But no matter how small the portion is, there always exists a heat flux passing through it and hence the local state is *not* isotropic. It is quite likely that the pressure tensor, for example, becomes anisotropic, and the equation of state is consequently modified. Then the local state cannot be identical to an equilibrium state, but should be described rather as a *local steady state*.

There has been some attempts to formulate thermodynamics for nonequilibrium steady states by going beyond local equilibrium treatments. See Sec. 1.3.5. Among these attempts, we regard the steady state thermodynamics (SST) proposed by Oono and Paniconi⁽²⁾ to be most sophisticated and promising. The basic strategy of Oono and Paniconi is to seek for a universal thermodynamic formalism respecting general mathematical structure of thermodynamics and operational definability of thermodynamic quantities. As far as we know, no other proposals of nonequilibrium thermodynamics follow such logically strict rules. Oono and Paniconi’s SST, however, is still too abstract to be tested empirically.

In the present paper, we follow the basic strategy of Oono and Paniconi’s, but try to construct much more concrete theory which leads to nontrivial predictions. Our strategy in the present work may be summarized as follows.

- Concentrate on some typical examples (i.e., a heat conducting fluid, a sheared fluid, and an electrically conducting fluid) of nonequilibrium steady states, always trying to elucidate universal aspects of the problem.
- Examine carefully how the basic notions of thermodynamics (for example, scaling, extensivity/intensivity, and operations to systems) should be modified in nonequilibrium steady states.

- Define every thermodynamic quantity through a purely operational procedure which can be realized experimentally.
- Make concrete predictions which may be checked experimentally to test our theory for its quantitative validity.

As a result, our theory has no direct logical connection with Oono and Paniconi's SST. But we keep the name SST to indicate that we share the basic philosophy with them.

Our theory is of course based on some phenomenological assumptions, the biggest one being the assumption that there exists a sensible thermodynamics. Although we are confident about theoretical consistency of our SST, its validity must ultimately be tested empirically.

If we restrict ourselves to certain idealized (but still nontrivial) theoretical models, we can demonstrate that the formalism of SST is indeed realized. We shall present such model dependent results as Appendices. The most complete "existence proof" is the results in Appendix B about the driven lattice gas, a standard stochastic model for nonequilibrium steady states. For a sheared fluid with a "weak coupling," we also recover a significant part (but, not the whole) of SST as we describe in Appendix A.

Of course we have no intention to claim that our SST should cover nonequilibrium states in general. Systems with explicit macroscopic time-dependence are out of consideration from the beginning. Systems which are too unstable to maintain stable thermodynamics cannot be treated. Moreover, since we make a full use of the pressure, model systems (such as chains of oscillators) which do not possess well-defined pressure do not fit into our scheme. We nevertheless hope that our formalism covers a generic and nontrivial class of nonequilibrium steady states.

The organization of this long paper may easily be read off from the table of contents. After discussing necessary materials from equilibrium physics in Sec. 2, we carefully describe our assumptions, and construct steady state thermodynamics step by step through Secs. 3–7. To help the readers, the beginning of each of these sections contains a brief summary of the section.

Before going into this massive main body, the reader is invited to take a look at the next Sec. 1.2, where we offer a very quick tour of our construction and predictions. In addition, we compare our approach with some of the existing attempts in Sec. 1.3, discuss possible experimental verifications in Sec. 8.2, and answer some of the "frequently asked questions" in Sec. 8.3. Appendices, which treat model dependent results, may be studied independently after reading the introductory Sec. 1.2.

We should better stress here that the present paper does *not* report a standard scientific research in which one provides answers to well established problems. We report our (admittedly ambitious) attempt to search for a novel universal framework that describes Nature. We thus take a nonstandard approach where we

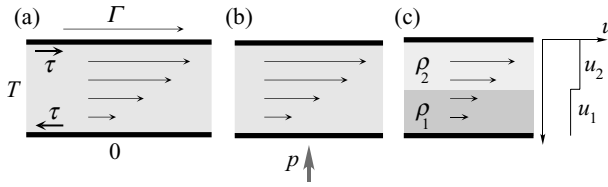


Fig. 1. (a) The nonequilibrium steady states of a sheared fluid. The velocity gradient is maintained by shear forces exerted on the fluid by the upper and the lower walls. The two walls exert exactly the opposite forces, whose magnitudes are τ , on the fluid. The steady state is parameterized as $(T, \tau; V, N)$. (b) The pressure is determined by measuring the vertical mechanical force exerted on the wall. (c) The chemical potential is determined by adding external potential to the system.

proceed step by step, stating each assumption carefully, examining its consistency, and discussing the consequences. We have tried our best to make the presentation as transparent as possible, not hiding any subtle points.

1.2. A Quick Look at Steady State Thermodynamics (SST)

To give the reader a rough idea about what our steady state thermodynamics is all about, we shall here outline (rather superficially) our construction and predictions in a single example of a sheared fluid. Every step illustrated here will be examined and explained carefully in latter sections of the paper. In particular we will thoroughly discuss in the latter sections why we believe that the present construction is essentially the unique way toward a sensible thermodynamics for nonequilibrium steady states.

1.2.1. Nonequilibrium Steady State in a Sheared Fluid

Suppose that N moles of fluid is contained in a box with the cross section area A and height h , and kept at a constant temperature T with the aid of an external heat bath. To make the state nonequilibrium, the upper wall of the box is moved horizontally with a constant speed Γ while the lower wall is kept at rest.³ We suppose that the walls are “sticky,” and the fluid will reach, after a sufficiently long time, a nonequilibrium steady state with a velocity gradient as in Fig. 1(a). We denote by τ the total horizontal force that the upper wall exerts on the fluid. The steadiness implies that the lower wall exerts exactly the opposite force on the fluid. Clearly the shear force τ measures the “degree of nonequilibrium” of the steady state.

³ It is convenient to imagine that periodic boundary conditions are imposed in the horizontal directions. Experimentally, one should modify the geometry (say, into a ring shape) to keep on moving the wall.

We shall parameterize the nonequilibrium steady state as $(T, \tau; V, N)$ where $V = Ah$ is the volume. As in the equilibrium thermodynamics (see Sec. 2.1), we frequently consider scaling, decomposition, and combination of steady states. In doing so, we always use the convention to fix the cross section area A constant, and vary only the height h .

In this convention of scaling, T and τ are identified as intensive variables, while V and N as extensive variables. These identifications are fundamental in our construction of SST.

We stress that the above convention of scaling and the choice of thermodynamic variables are results of very careful examination of general structures of thermodynamics and the characters specific to nonequilibrium steady states. These points are discussed in Secs. 3 and 4.

1.2.2. Pressure and Chemical Potential

We now fix the two intensive parameters T and τ , and determine the pressure $p(\rho)$ and the chemical potential $\mu(\rho)$ as functions of the density $\rho = V/N$. We insist on determining these quantities in a purely operational manner, only using procedures that can be realized experimentally. This is the topic of Sec. 5.

The pressure $p(\rho)$ is simply defined as the mechanical pressure on the lower or the upper wall as in Fig. 1(b). In other words we concentrate on the vertical component of the pressure.

The measurement of the chemical potential $\mu(\rho)$ requires extra cares. We (fictitiously) divide the system into half along a horizontal plane, and apply a potential which is equal to u_1 in the lower half and equal to u_2 in the upper half. We denote by ρ_1 and ρ_2 the densities in the lower and the upper parts, respectively, in the steady state under the potential. We shall define the SST chemical potential $\mu(\rho)$ as a function which satisfies

$$\mu(\rho_1) + u_1 = \mu(\rho_2) + u_2, \quad (1.1)$$

for any u_1 and u_2 .

Note that this only determines the difference of $\mu(\rho)$. There remains a freedom to add an arbitrary constant to $\mu(\rho)$. In other words, we have determined the V, N dependence of the chemical potential, but not T, v dependence.

An essential point of these definitions is that the Maxwell relation

$$\frac{\partial p(\rho)}{\partial \rho} = \rho \frac{\partial \mu(\rho)}{\partial \rho} \quad (1.2)$$

can be shown to hold in general.

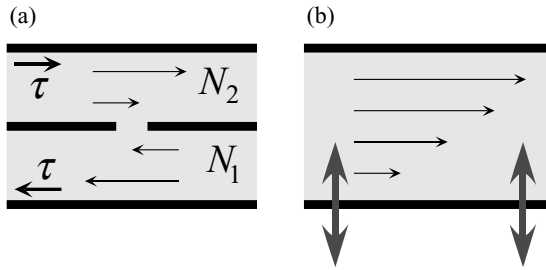


Fig. 2. Two basic applications of the SST free energy $F(T, \tau; V, N)$. (a) We conjecture that Einstein’s formula for density fluctuation extends to nonequilibrium steady states, provided that the two regions are separated by a wall with a window in it. (b) The minimum work principle is conjectured to hold when the agent is only allowed to move horizontal walls vertically.

1.2.3. Helmholtz Free Energy

Since we have determined the pressure and the chemical potential, we can introduce and investigate the SST free energy. This is done in Sec. 6. We define the specific free energy through the Euler equation as

$$f(\rho) = -p(\rho) + \rho \mu(\rho). \tag{1.3}$$

The extensive free energy is obtained as $F(T, \tau; V, N) = V f(N/V)$. We have thus operationally determined the V, N dependence of $F(T, \tau; V, N)$ for each T and τ .

We make three predictions which involve the V, N dependence of the free energy. The first two of these phenomenological conjectures can be verified by making plausible assumption about contact, as we shall see in Appendix B.3.4. In a class of stochastic processes treated in Appendix , all the three conjectures are derived.

The first prediction is an extension of Einstein’s formula on macroscopic density fluctuation. Consider the steady state $(T, \tau; 2V, 2N)$ with $2N$ moles of fluid in a box with volume $2V$. We divide the system into two identical parts with volumes V by a horizontal wall with a small window⁴ in it as in Fig. 2(a). We fix the wall in the middle, and apply the same shear force τ to the upper and the lower walls to maintain the constant shear in the whole system. In this way the two parts are coupled weakly and exchange fluid molecules. Let N_1 and N_2 be the amounts of fluid in the lower and the upper parts, respectively. Although both N_1 and N_2 should be equal to N in the average, one always observes a fluctuation in a finite system. Our conjecture is that the probability $\tilde{p}(N_1, N_2)$ of observing N_1 and N_2

⁴ See Appendix B.3.4 for details about the window.

moles of fluid in the two parts is given by

$$\tilde{p}(N_1, N_2) \propto \exp \left[-\frac{1}{k_B T} \{F(T, \tau; V, N_1) + F(T, \tau; V, N_2)\} \right], \quad (1.4)$$

where k_B is the Boltzmann constant. Unlike the corresponding relation in equilibrium, this relation is expected to hold only when the two regions are separated by the horizontal wall with a window.

The second prediction is the fluctuation-response relation for time-dependent processes that takes place in the same setting as above. We shall leave details to Secs. 6.2, A.4, and B.6.

The third prediction is an extension of the minimum work principle, a version of the second law of thermodynamics. Suppose that an outside agent moves one of the horizontal walls of the box vertically, always keeping the wall horizontal as in Fig. 2(b). We assume that T and τ are kept constant during the operation. We denote by V and V' the initial and the final volumes, respectively. Denoting by W the total mechanical work done by the agent, we can write the conjectured minimum work principle for nonequilibrium steady states as

$$W \geq F(T, \tau; V', N) - F(T, \tau; V, N), \quad (1.5)$$

which has exactly the same form as the corresponding equilibrium relation. An essential difference is that we here severely restrict allowed operations.

1.2.4. Flux-Induced Osmosis and Shift of Coexistence Temperature

We shall now determine the SST free energy $F(T, \tau; V, N)$ completely and make further conjectures. This is the topic of Sec. 7.

The key idea is to consider the setting in Fig. 3(a), where a nonequilibrium steady state $(T, \tau; V, N)$ with a finite shear is in contact with an equilibrium state $(T, 0; V', N')$ via a porous wall. Since the two states can exchange fluid, we require that

$$\mu(T, \tau; V, N) = \mu(T, 0; V', N') \quad (1.6)$$

as in equilibrium thermodynamics. Since $\mu(T, 0; V', N')$ is an already known equilibrium quantity, we use (1.6) as the definition of the SST chemical potential.

Now that the chemical potential has been fully determined, we can also determine the SST free energy $F(T, \tau; V, N)$ through (1.3), including its dependence on T and τ . Then we can define the SST entropy

$$S(T, \tau; V, N) = -\frac{\partial}{\partial T} F(T, \tau; V, N), \quad (1.7)$$

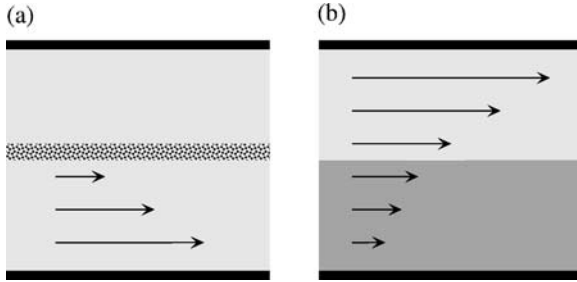


Fig. 3. (a) A nonequilibrium steady state with a finite shear is in contact with an equilibrium state without a shear. The two states are separated by a porous wall that allows fluid to pass through. The top wall and the porous wall are at rest while the bottom wall has a constant horizontal velocity. This setup is used to determine the chemical potential and the free energy completely. SST leads to a conjecture that the (vertical) pressure in the steady state is always larger than that in the equilibrium state. (b) A nonequilibrium steady state with a phase coexistence. We conjecture that the coexistence temperature $T_c(p, \tau)$ deviates from that in the equilibrium.

and a new extensive quantity

$$\Psi(T, \tau; V, N) = -\frac{\partial}{\partial \tau} F(T, \tau; V, N). \tag{1.8}$$

We call $\Psi(T, \tau; V, N)$ the nonequilibrium order parameter, since we can show (under the assumption about concavity of $F(T, \tau; V, N)$ in τ) that $\Psi(T, 0; V, N) = 0$ and $\Psi(T, \tau; V, N) = -\Psi(T, -\tau; V, N) \geq 0$ if $\tau \geq 0$.

The nonequilibrium order parameter $\Psi(T, \tau; V, N)$ characterizes two important phenomena, which are intrinsic to nonequilibrium steady states.

The first phenomenon takes place in the setting of Fig. 3(a). Suppose one fixes the pressure p_{eq} of the equilibrium part, and changes the shear force τ . Then we can show that the pressure p_{ss} of the steady state satisfies

$$\frac{\partial p_{ss}}{\partial \tau} = \frac{\Psi(T, \tau; V, N)}{V}. \tag{1.9}$$

Since $p_{ss} = p_{eq}$ when $\tau = 0$, this (and the knowledge about the sign of Ψ) implies that $p_{ss} \geq p_{eq}$ in general. We expect that $p_{ss} > p_{eq}$ holds for $\tau \neq 0$. The steady state always has a higher pressure than the equilibrium state. We call this pressure difference the flux-induced osmosis (FIO). Note that FIO can never be predicted within the standard local equilibrium treatments.

To see the second phenomenon, suppose that two phases (such as gas and liquid) coexist within a steady state as in Fig. 3(b). We denote by $T_c(p, \tau)$ the temperature at which the coexistence takes place when the pressure and the shear

force are fixed at p and τ , respectively. We can then show that

$$\frac{\partial T_c(p, \tau)}{\partial \tau} = -\frac{\Psi_g - \Psi_\ell}{S_g - S_\ell}, \quad (1.10)$$

where $S_{g,\ell}$ and $\Psi_{g,\ell}$ are the entropy and the nonequilibrium order parameter in the gas and the liquid phases, respectively. This means that in general the coexistence temperature $T_c(p, \tau)$ in a nonequilibrium steady state is different from that in equilibrium. This, again, is a truly nonequilibrium phenomenon. Applied to the phase coexistence between a fluid and a solid phases, the same argument yields $T_c(p, \tau) < T_c(p, 0)$. Thus the shear induces melting.

It is important that the same quantity Ψ plays the essential roles in the above two phenomena. This means that we can test the quantitative validity of SST through purely experimental studies.

1.3. Existing Approaches to Nonequilibrium Steady States

In the present section, we briefly discuss some of the existing approaches to nonequilibrium steady states, and see how they are (or how they are not) related to our own approach of SST. We note that the aim here is not to give an exhaustive and balanced review of the field, but to place our new work in the context of (necessarily biased) summary of nonequilibrium thermodynamics and statistical mechanics.

1.3.1. Phenomenological Theories in the Linear Nonequilibrium Regime

Probably the best point to start this discussion on nonequilibrium physics is Einstein's celebrated work on the Brownian motion. We have no intention of going deeply into the work, but wish to mention that Einstein's formula

$$D = k_B T \mu, \quad (1.11)$$

derived in Refs. 5 and 6 represents a deep fact that the transport coefficient (the mobility μ) in a driven nonequilibrium state is directly related to the diffusion constant D , which characterizes fluctuation in the equilibrium state.

(a) *Onsager's theory*: Such a relation between equilibrium fluctuation and nonequilibrium transport was stated as a fundamental principle of (linear) nonequilibrium physics by Onsager. In his famous paper on the reciprocal relations,⁽⁷⁾ he formulated the *regression hypothesis* which asserts that "the average regression of fluctuations (in equilibrium) will obey the same laws as the corresponding macroscopic irreversible processes."⁽⁸⁾ From the regression hypothesis and microscopic reversibility of underlying mechanics, Onsager^(7,8) derived the reciprocal relations for transport coefficients. Since the reciprocal relations are established

experimentally, this provides a strong support to the regression hypothesis, at least in the linear nonequilibrium regime. It is fair to say that, as far as nonequilibrium steady states in linear transport regime are concerned, Onsager constructed a beautiful phenomenology with sound theoretical and empirical bases.

Onsager's theory is essentially related to (at least) three subsequent developments in nonequilibrium physics that we shall discuss in the following.

(b) *Linear response relations*: A series of formulae that express various transport coefficients in terms of time-dependent equilibrium correlation functions was found in various contexts, the first example being that by Nyquist,⁽⁹⁾ who precedes Onsager. These formulae are now known under the generic name *linear response relations*. See, for example Refs. 10 and 11. We believe that the conceptual basis of these relations should be sought in a certain form of regression hypothesis, i.e., quantitative correspondence between nonequilibrium transport and equilibrium fluctuation.

(c) *Variational principles*: The second development is the establishment of variational principles which relate currents to the corresponding forces in the linear response regime. The simplest version of such principles, called the *principle of the least dissipation of energy*, is obtained as a direct consequence of the reciprocal relations.^(7,8) Another type of variational principle attempting to characterize nonequilibrium steady states is called the *principle of minimum entropy production*.⁽¹²⁾ It is understood that all the correct variational principles in linear transport regime are based on the Onsager-Machlup theory^(13–15) which concerns a large deviation functional for the history of fluctuations. See, for example Ref. 16.

(d) *Nonequilibrium thermodynamics*: Flux-force relations with the reciprocity constitute fundamental ingredients of the standard theory known as nonequilibrium thermodynamics, which provides a macroscopic description of a system which slightly deviates from equilibrium.^(12,17) A fundamental assumption in this approach is that a small portion of the system in the nonequilibrium state can be regarded as a *local equilibrium state* in the sense that all the thermodynamic relations in equilibrium (not only universal relations, but also equations of states specific to each system) are valid without modifications. One then allows macroscopic thermodynamic variables to vary slowly in space and time, assuming that there takes place linear transport according to a given set of transport coefficients.

(e) *Relation to SST*: We wish to see how our SST is related to these theories. In short, we see no direct logical connection for the moment. All of these theories are essentially limited to linear transport regime with very small “degree of nonequilibrium,” while SST is designed to apply to any nonequilibrium steady states. The variational principles mentioned above attempt to characterize the steady state itself, while the SST free energy mainly describes the response of nonequilibrium steady states to external operations (such as the change of the volume) under a fixed degree of nonequilibrium. We can say that, at least for the moment, SST covers aspects complimentary to that dealt with the above theories.

It would be very interesting to incorporate Onsager's and related phenomenology into SST, but we do not yet see how this can be accomplished.

We have already stressed in Sec. 1.1 the difference between the nonequilibrium thermodynamics and our SST. Our main motivation is to construct thermodynamics that applies to systems very far from equilibrium. We must abandon the description in terms of local equilibrium states, and replace it with that in terms of local steady states.⁵

1.3.2. Approaches from Microscopic Dynamics

It is a natural idea to realize and characterize nonequilibrium steady states by using equilibrium states and microscopic (classical or quantum) dynamics. Suppose that we are interested in a heat conducting steady state. We prepare an arbitrary (macroscopic) subsystem, and couple it to two "heat baths" which are much larger than the subsystem. The two heat baths are initially in thermal equilibria with different temperatures. We then let the whole system evolve according to the microscopic equation of motion. After a sufficiently long (but not too long) time, the subsystem is expected to reach a steady heat conducting state. By projecting only onto the subsystem, we get the desired nonequilibrium steady state. If such a projection can be executed for general systems, there is a chance that we can extract a universal description for nonequilibrium steady states.

Of course the procedure described above is in general too difficult to be carried out literally even in the linear response regime. We shall see two approximate calculation schemes within the conventional statistical mechanics (which are (a) and (b)), and some of more mathematical approaches (which are (c), (d), and (e)).

If and when these theories provide us with concrete information about the structure of nonequilibrium steady states and their response to external operations, we can (and should) check the consistency between such predictions and those obtained from SST. For the moment most of the known results are rather formal, and we do not find any concrete results which should be compared with SST.

(a) *Linear response theory*: Probably the most well-known of such schemes is the linear response theory.^(10,11) Although this theory is sometimes referred to as a "microscopic (or rigorous) derivation" of linear response relations (see, for example Ref. 10), it is after all a formal perturbation theory about the equilibrium state, and does not deal with the intrinsic characterization of nonequilibrium steady states. As far as we understand, certain phenomenological principle must be invoked to justify such a derivation.

⁵ It should be noted that, in the present work, we are concentrating on characterizing local steady states, and not yet considering spatial and temporal variation of macroscopic variables. It is among our future plan to patch together local steady states to describe non-uniform nonequilibrium states.

(b) *Methods based on the Liouville equation:* In classical mechanics, the Liouville equation can be a starting point for microscopic considerations. An example is the derivation of the non-linear response relation of Ref. 18, which leads to the Kawasaki-Gunton formula⁽¹⁹⁾ for a nonlinear shear viscosity and normal stresses. Another example is the establishment of the existence of long range spatial correlations of fluctuations in nonequilibrium steady states.⁽²⁰⁾ These results were obtained by employing the projection operator method pioneered by Zwanzig⁽²¹⁾ and Mori.⁽²²⁾ Furthermore, through a formal argument based on the Liouville equation, McLennan⁽²³⁾ and Zubarev⁽²⁴⁾ proposed a measure that describes (or is claimed to describe) nonequilibrium states.

Although the derivations of these results involve (often uncontrolled) assumptions, the nonlinear response relation, the Kawasaki-Gunton formula, and the power-law decay of spatial correlations are believed to be physically sound, since they can also be derived in simple manners from phenomenological considerations. See Ref. 25 for the nonlinear response relation,⁽²⁶⁾ for the Kawasaki-Gunton formula, and Ref. 20 for the long range correlations. The measure proposed by McLennan and Zubarev is supported by neither a controlled theory nor a phenomenological argument. It is therefore difficult to judge its physical validity and usefulness.

(c) *Weak coupling limit:* In the weak coupling limit of quantum systems, the procedure of projection can be executed rigorously.⁽²⁷⁾ Relaxation to the steady state, the reciprocal relations in linear transport, and the principle of minimum entropy production are established. In this study, however, explicit forms of nonequilibrium steady states are not obtained.

(d) *C* algebraic approaches:* There is a series of works in which heat baths are modeled by infinitely large systems of ideal gases, and the time evolution is discussed by using the C* algebraic formalism. See, for example Ref. 28. As far as we understand, the results obtained in this direction mainly focus on what happens when more than two baths are put into contact, rather than what happens in the subsystem where transport is taking place. We still do not get much information about the structure of nonequilibrium steady states from these works.

(e) *Chain of anharmonic oscillators* A standard model for heat conduction in classical mechanics is the chain of coupled anharmonic oscillators whose two ends are attached to two heat baths with different temperatures. From numerical simulations (see, for example Ref. 29) it is expected that the model exhibits a “healthy” heat conduction, i.e., obeys the Fourier law. Mathematically, basic results including the existence, uniqueness and mixing property of the nonequilibrium steady states are proved under suitable conditions,^(30,31) but no concrete information about the structure of the heat conducting state is available. Recently a new perturbative method for the nonequilibrium steady state of this model was developed.⁽³²⁾

1.3.3. Approaches from Meso-Scale Models

We turn to approaches to nonequilibrium steady states that employ a class of models which are neither microscopic (as in mechanical treatments) nor macroscopic (as in thermodynamic treatments). The class, which may be called mesoscopic, includes the Boltzmann equation, the nonlinear Langevin equations for slowly varying macroscopic variables, and the driven lattice gas.

(a) *Boltzmann equation*: The method developed by Chapman and Enskog⁽³³⁾ enables one to explicitly compute perturbative solutions of the Boltzmann equation. Expecting that the Boltzmann equation, which was originally introduced to describe relaxation to equilibrium, may be extended to study nonequilibrium phenomena,⁶ nonequilibrium stationary distribution functions have been calculated. Recently, for example, a systematic calculation for heat conducting nonequilibrium steady states was performed.^(35,36) Such a study reveals detailed properties of the nonequilibrium steady states, and may become an important guide in construction of phenomenology and statistical mechanical theory. The relation of this result to SST will be discussed in Sec. 7.4. As for recent progress in this direction, see Refs. 35 and 36.

(b) *Nonlinear Langevin model for macroscopic variables*: Nonlinear Langevin models for macroscopic variables were useful to study anomalous behavior of transportation coefficients at the critical point.⁽³⁷⁾ The shift of the critical temperature under the influence of shear flow as well as the corresponding critical exponents were calculated by analyzing the so called model H with the steady shear flow.⁽³⁸⁾

Such an approach might produce correct results for universal quantities (such as the critical exponents) which are insensitive to minor details of models. It is questionable, however, whether a non-universal quantity like the critical temperature shift can be properly dealt with. Results from a model calculation may be always improved by making the model more and more complicated, but such a process of improvement seems endless. If the formulation of SST is true, on the other hand, the shift of coexistence temperatures should be related to other measurable quantities through the (conjectured) extended Clapeyron law, which is expected to be universal.⁷

⁶The Boltzmann equation can be derived from the BBGKY hierarchy in a low density limit around the (spatially uniform) equilibrium state. (See Ref. 34 for the mathematical justification of the derivation.) We have to keep in mind, however, that there is a logical possibility that correction terms to the Boltzmann equation appear in the truncation process from the BBGKY hierarchy when the spatial non-uniformity of the states are taken into account.

⁷Needless to say, thermodynamic phases may be in principle determined from microscopic descriptions when and if statistical mechanics for nonequilibrium steady states is constructed.

(c) *Driven lattice gas*: Given the history that the lattice gas models (equivalently, the Ising model) was the paradigm model in the study of equilibrium phase transitions, it is natural that various stochastic models of lattice gases for nonequilibrium states were studied. See, for example, Ref. 39. The simplicity of these models made it possible to resolve some delicate issues rigorously, a notable examples being the long-range correlations⁽⁴⁰⁾ and the anomalous current fluctuation.⁽⁴¹⁾

A standard nontrivial model is the driven lattice gas,⁽⁴²⁾ in which particles on lattice are subject to hard core on-site repulsion, nearest neighbor interaction, and a constant driving force. Many results, both theoretical and numerical, have been obtained,^(39,43) but the structure of the nonequilibrium steady state is still not very well understood except for some partial results including the recent perturbation expansion.⁽⁴⁴⁾ In Ref. 45 hydrodynamic limit and fluctuation was studied for the nonequilibrium steady state in the driven lattice gas. Possibility of thermodynamics of driven lattice gas being “shape-dependent” was pointed out in Ref. 46. In SST, such a shape-dependence is properly taken into account in the basic formalism.

For us the driven lattice gas provides a very nice “proving ground” for various proposals and conjectures of SST. Some of our discussions in the present paper are based on earlier numerical works by Hayashi and Sasa.⁽⁴⁷⁾ In Appendix of the present paper, we also discuss theoretical results about SST realized in driven lattice gases.

In spite of all these interesting works, we always have to keep in mind that physical basis of these stochastic lattice models are still unclear. As for the stochastic dynamics near equilibrium, it is well appreciated that the detailed balance condition (which was indeed pointed out in Onsager’s work on the reciprocal relations⁽⁷⁾) is the necessary and sufficient condition to make the model physically meaningful. As for dynamics far away from equilibrium, we still do not know of any criteria that should replace the detailed balance condition.

1.3.4. Recent Progress

In the last decade, there have been some progress in new directions of study on nonequilibrium steady states. They are fluctuation theorem, additivity principle, and dynamical fluctuation theory. We shall briefly review them and comment on the relevance to SST.

(a) *Fluctuation theorem*: In a class of chaotic dynamical systems, a highly nontrivial symmetry in the entropy production rate, now known by the name *fluctuation theorem*, was found.^(48,49) The fluctuation theorem was then extended to nonequilibrium steady states in various systems.^(50–52)

Now it is understood that the essence of the fluctuation theorem lies in the fact that the relevant nonequilibrium steady states are described by Gibbs measures for space-time configurations.⁽⁵²⁾ It is known that nonequilibrium steady states that are modeled by a class of chaotic dynamical system⁽⁴⁾ or by a class of stochastic processes^(51,53) are described by space-time Gibbs measures. But it is not yet clear if the description in terms of a space-time Gibbs measure is universally valid.

A more important question is whether a space-time description is really necessary for nonequilibrium steady states. One might argue that any nonequilibrium physics should be described in space-time language, since the time-evolution must play a crucial role. On the other hand, one may also expect that the temporal axis is redundant for the description of nonequilibrium *steady* states since nothing depends on time.

Our formalism of SST is based on the assumption that one can construct a consistent macroscopic phenomenology without explicitly dealing with the temporal axis. If a space-time description is mandatory for nonequilibrium physics, our attempt should reveal its own failure as we pursue it. So far we have encountered no inconsistencies.

(b) *Additivity principle*: Recently Derrida, Lebowitz, and Speer obtained exact large deviation functionals for the density profiles in the nonequilibrium steady states of the one dimensional lattice gas models (the symmetric exclusion process^(54,55) and the asymmetric exclusion process^(56,57)) attached to two particle baths with different chemical potentials. In the equilibrium states, the corresponding large deviation functional coincides with the thermodynamic free energy. Moreover their large deviation functional satisfies a very suggestive variational principle named *additivity principle*. It was further proposed⁽⁵⁸⁾ that, in a large class of one dimensional models, the large deviation functional for current satisfies a similar additivity principle.

It would be quite interesting if these large deviation functionals could be related to the SST free energy that we construct operationally. Unfortunately we still do not see any explicit relations. A difficulty comes from the restriction to one dimensional lattice systems, where it is not easy to realize macroscopic operations which are essential in our construction. It is thus of great interest whether the additivity principles can be extended to higher dimensions.

(c) *Dynamical fluctuation theory*: Bertini, De Sole, Gabrielli, Jona-Lasinio, and Landim^(59,60) re-derived the above mentioned large deviation functional by analyzing the model of fluctuating hydrodynamics. In Refs. 59 and 60, the large deviation functional of the density profile is obtained through the history minimizing an action functional for spontaneous creation of a fluctuation. When one is concerned with equilibrium dynamics, which has the detailed balance property, such a task can be accomplished essentially within the Onsager–Machlup theory.⁽¹⁴⁾ In nonequilibrium dynamics, where the detailed balance condition is explicitly violated, a modified version of the Onsager–Machlup theory had to be devised to

derive a closed equation⁸ for the large deviation functional.^(59,60) By using the equation, the possible form of the evolution of fluctuations was determined, and a generalized type of fluctuation dissipation relation for nonequilibrium steady states was proposed.

In Refs. 59 and 60 the form of fluctuating hydrodynamics must be assumed or derived from other microscopic models. We believe that the SST free energy, if it really exists, should be taken into account in this step. It would be quite interesting if the fluctuation dissipation relation that they proposed is related to the generalized second law of our SST.

1.3.5. Thermodynamics Beyond Local Equilibrium Hypothesis

There of course have been a number of attempts to formulate nonequilibrium thermodynamics that goes beyond local equilibrium treatment.⁹ A considerable amount of works appear under the name *extended irreversible thermodynamics*.^(63,64)

In extended irreversible thermodynamics, thermodynamic functions with extra variables for the “degree of nonequilibrium” are considered, and thermodynamic relations are discussed for various systems. This is quite similar to what we shall do in our own SST.

As far as we have understood, however, the philosophies behind extended irreversible thermodynamics and our SST are very much different. In the literature of extended irreversible thermodynamics, we do not find anything corresponding to our careful (and lengthy) discussions about the convention of scaling, the identification of intensive and extensive variables, the (almost) unique choice of nonequilibrium variables, the fully operational construction of the free energy, or the proof of Maxwell relation. We also notice that, in many works in the extended irreversible thermodynamics, different levels of approaches, such as macroscopic phenomenology, microscopic kinetic theory, and statistical mechanics (such as the maximum entropy method) are discussed simultaneously. In our own approach

⁸ Unfortunately, it is likely that the equations for the large deviation functional can be solved exactly only in special cases, the model treated by Derrida, Lebowitz, and Speer being an example.

⁹ Landauer^(61,62) made a deep criticism to thermodynamics and statistical mechanics for nonequilibrium states in general. He argued, correctly, that one cannot expect to fully characterize a nonequilibrium state by simply minimizing a local function of states like the energy or the free energy. The main point of his argument is that a coupling between two different subsystems can be much more delicate and trickier than we are used to in equilibrium physics.

We can assure that our SST is perfectly safe from Landauer’s criticism. First of all, we ourselves have encountered the delicateness of variational principle in nonequilibrium steady states, and this observation led us to the (almost) unique choice of nonequilibrium thermodynamic variables. This point will be discussed in Sec. 4.2. Delicateness of contact is another issue that we ourselves have realized (with a surprise) during the development of SST. In Sec. 7.5, we shall argue that the contact between an equilibrium state and a nonequilibrium steady state may be very delicate.

to SST, in contrast, we have tried to completely separate thermodynamics from microscopic considerations, stressing what outcome we get (and we do not get) from purely macroscopic phenomenology.

Although it is impossible to examine all the existing literature, it is very likely that more or less the same comments apply to other approaches in similar spirit. Examples include

To make the comparison more concrete, let us take a look at two examples.

The same problem of sheared fluid that we have briefly seen in Sec. 1.2 is treated, for example, in Refs. 68 and 69. Although the final conclusion⁽⁶⁹⁾ that shear induces melting is the same, everything else is just different. The discussion in Refs. 68 and 69 are essentially model dependent, while we try to derive universal thermodynamic relations. Moreover the proposed thermodynamics in Refs. 68 and 69 uses the shear velocity Γ (more precisely the shear rate $\dot{\gamma} = \Gamma/h$ where h is the distance between the upper and the lower walls) as the nonequilibrium variable. But one of our major conclusions in the present work is that a thermodynamics with the variable Γ (or $\dot{\gamma}$) has a pathological behavior. Thus the analysis of Refs. 68 and 69 can never be consistent with our SST. Indeed it is our opinion that the introduction of the nonequilibrium entropy in Ref. 70 which gives a foundation to the above works, is not well-founded. Analysis of sheared fluids in Refs. 71 and 72 looks sounder to us, but still does not contain careful steps as in SST.

In Ref. 73 the pressure in a heat conducting state is discussed. This again is in a sharp contrast between our own discussion of a similar problem. The work in Ref. 73 is based on a formula of the Shannon entropy obtained from microscopic theories (kinetic theory and the maximum entropy calculation). We see no reason that the Shannon entropy gives meaningful thermodynamic entropy once the system is away from equilibrium. Operational meaning of the pressure is also unclear. A gedanken experiment is proposed, but there seems to be no way of realizing this setting (even in principle) unless one precisely knows in advance the formula for the nonequilibrium pressure. Our discussion, in contrast, starts from a completely operational definition of the pressure. We also predict a shift of pressure due to nonequilibrium effects in Sec. 7.4, but as a universal thermodynamic relation. Let us note in passing that the maximum entropy calculation (called information theory), on which Ref. 73 and other related works rely (see also, Ref. 74), is found to produce results which are inconsistent with the Boltzmann equation (36).

To conclude, our SST is completely different in essentially all the aspects from the extended irreversible thermodynamics and other similar approaches. The only similarity is in superficial formalism, i.e., thermodynamic functions with extra variables. It is our belief that our own approach achieves much higher standard of logical rigor, and has a better chance of providing truly powerful and correct description of nature.

2. BRIEF REVIEW OF EQUILIBRIUM PHYSICS

Before dealing with nonequilibrium problems, we present a very brief summary of thermodynamics (Sec. 2.1), statistical mechanics (Sec. 2.2), and approaches based on stochastic processes (Sec. 2.3) for equilibrium systems. The main purpose of the present section is to fix some notations and terminologies used throughout the paper, to give some necessary background, and, most importantly, to motivate our approach to steady state thermodynamics (SST).

2.1. Equilibrium Thermodynamics

Equilibrium thermodynamics is a universal theoretical framework which applies *exactly* to arbitrary macroscopic systems in equilibrium.

Here we restrict ourselves to the formalism of equilibrium thermodynamics at a fixed temperature, since it is directly related to our approach to steady state thermodynamics. See, for example Ref. 75 for relations between different formalisms of thermodynamics.¹⁰

2.1.1. Equilibrium States and Operations

A fluid consisting of a single substance of amount¹¹ N is contained in a container with volume V and kept in an environment with a fixed temperature T . If we leave the system in this situation for a sufficiently long time, it reaches an equilibrium state, where no observable macroscopic changes take place. An equilibrium state of this system is known to be uniquely characterized (at least in the macroscopic scale) by the three macroscopic parameters T , V , and N . We can therefore denote the equilibrium state symbolically as $(T; V, N)$. Note that we have separated the intensive variable T and the extensive variables V, N by a semicolon. This convention will be used throughout the present paper.

In thermodynamics, various operations to equilibrium states play essential roles. Let us review them briefly.

By gently inserting a thin wall into an equilibrium state, one can *decompose* the state into two separate equilibrium states. This is symbolically denoted as

$$(T; V, N) \rightarrow (T; V_1, N_1) + (T; V_2, N_2), \quad (2.1)$$

¹⁰The most beautiful formalism of thermodynamics uses energy variable instead of temperature. See, for example Ref. 3.

¹¹The amount of substance N is sometimes called the “molar number” since N is usually measured in moles.

where¹² $V_1 + V_2 = V$ and $N_1 + N_2 = N$. One may realize the inverse of this operation by attaching the two equilibrium states together and removing the wall between them. Another important operation is to put two or more equilibrium states together, separating them by walls which do not pass fluids but are thermally conducting. In this way we get an equilibrium state characterized by a single temperature T and more than one pairs of (V, N) .

Given an arbitrary $\lambda > 0$, one can associate with an equilibrium state $(T; V, N)$ its *scaled copy* as

$$(T; V, N) \rightarrow (T; \lambda V, \lambda N). \quad (2.2)$$

The scaled copy has exactly the same properties as the original state, but its size has been scaled.

The intensive variable T and the extensive variables V, N show completely different behaviors under the operations (2.1) and (2.2). One may roughly interpret that an intensive variable characterizes a certain property of the environment of the system, while an extensive variable measures an amount of the system.

2.1.2. Helmholtz Free Energy

The Helmholtz free energy (hereafter abbreviated as “free energy”) $F(T; V, N)$ is a special thermodynamic function which carries essentially all the information regarding the equilibrium state $(T; V, N)$.

The free energy $F(T; V, N)$ is *concave* in the intensive variable T , and is jointly *convex*¹³ in the extensive variables V and N . Corresponding to the decomposition (2.1), it satisfies the *additivity*

$$F(T; V, N) = F(T; V_1, N_1) + F(T; V_2, N_2), \quad (2.3)$$

and corresponding to the scaling (2.2), the *extensivity*

$$F(T; \lambda V, \lambda N) = \lambda F(T; V, N). \quad (2.4)$$

The free energy $F(T; V, N)$ appears in the second law of thermodynamics in the form of the minimum work principle. Consider an arbitrary mechanical operation to the system executed by an external (mechanical) agent, a typical (and important) example being a change of volume caused by the motion of a wall. We assume that the system is initially in the equilibrium state $(T; V, N)$, and the operation is done in an environment with a fixed temperature T . Sufficiently long time after the operation, the system will settle down to another equilibrium state

¹²Note that V_1, V_2, N_1, N_2 in the right-hand side are not arbitrary. If one fixes (for example) V_1, V_2 , then N_1, N_2 are determined almost uniquely.

¹³A function $g(V, N)$ is jointly convex in (V, N) if $g(\lambda V_1 + (1 - \lambda)V_2, \lambda N_1 + (1 - \lambda)N_2) \leq \lambda g(V_1, N_1) + (1 - \lambda)g(V_2, N_2)$ for any V_1, V_2, N_1, N_2 , and $0 \leq \lambda \leq 1$.

$(T; V', N)$. Let W be the total mechanical work done by the agent during the whole operation. Then the *minimum work principle* asserts that the inequality

$$W \geq F(T; V', N) - F(T; V, N) \tag{2.5}$$

holds for an arbitrary operation. Note that the operation need not be gentle or slow.

Another important physical relation involving the free energy is the following formula about fluctuation in equilibrium. Suppose that we have two systems of the same volume V which are in a weak contact with each other which allows fluid to move from one system to another slowly. If the total amount of fluid is $2N$, the amount of substance in each subsystem should be equal to N in average. But there always is a small fluctuation in the amount of substance. Let $\tilde{p}(N_1, N_2)$ be the probability density that the amounts of substance in the two subsystems are N_1 and N_2 . Then it is known that in equilibrium this probability behaves as

$$\tilde{p}(N_1, N_2) \propto \exp \left[-\frac{1}{k_B T} \{F(T; V, N_1) + F(T; V, N_2)\} \right], \tag{2.6}$$

where k_B is the Boltzmann constant. This is the isothermal version of Einstein's celebrated formula of fluctuation. See, for example, chapter XII of Ref. 76.

2.1.3. Variational Principles and Other Quantities

Let $V_1, V_2, N_1,$ and N_2 be those in the decomposition (2.1). Then from the extensivity (2.4) and the convexity of $F(T; V, N)$, one can show the variational relation¹⁴

$$F(T; V_1, N_1) + F(T; V_2, N_2) = \min_{\substack{V'_1, V'_2 \\ (V'_1 + V'_2 = V)}} \{F(T; V'_1, N_1) + F(T; V'_2, N_2)\}, \tag{2.7}$$

which corresponds to the situation in which the system is divided by a movable wall into two parts with fixed amounts N_1 and N_2 of fluids. The volumes V'_1 and V'_2 of the two parts can vary within the constraint $V'_1 + V'_2 = V$, and finally settle to the equilibrium values V_1 and V_2 , respectively. If we define the *pressure* by

$$p(T; V, N) = -\frac{\partial F(T; V, N)}{\partial V}, \tag{2.8}$$

¹⁴The derivation is standard, but let us describe it for completeness. Let $N = N_1 + N_2$ and $\lambda = N_1/N$, and take arbitrary V'_1, V'_2 with $V'_1 + V'_2 = V$. Then from the extensivity (2.4) and the convexity (see footnote 13), we get $F(T; V'_1, N_1) + F(T; V'_2, N_2) = \lambda F(T; V'_1/\lambda, N) + (1 - \lambda) F(T; V'_2/(1 - \lambda), N) \geq F(T; V, N)$. With the additivity (2.3), this implies a variational principle (2.7).

the variational relation (2.7) leads to the condition

$$p(T; V_1, N_1) = p(T; V_2, N_2), \quad (2.9)$$

which expresses the mechanical balance between the two subsystems (that have volumes V_1 and V_2 , respectively). This thermodynamic pressure coincides with the pressure defined in a purely mechanical manner.¹⁵

One can derive the similar variational relation

$$F(T; V_1, N_1) + F(T; V_2, N_2) = \min_{\substack{N'_1, N'_2 \\ (N'_1 + N'_2 = N)}} \{F(T; V_1, N'_1) + F(T; V_2, N'_2)\}, \quad (2.10)$$

for the situation where the system is divided into two parts with fixed volumes V_1 , V_2 , and the amounts N'_1 and N'_2 in the two parts may vary within the constraint $N'_1 + N'_2 = N$. This leads to another balance condition

$$\mu(T; V_1, N_1) = \mu(T; V_2, N_2), \quad (2.11)$$

where

$$\mu(T; V, N) = \frac{\partial F(T; V, N)}{\partial N} \quad (2.12)$$

is the *chemical potential*.

To get a better insight about the chemical potential, and to motivate our main definition of the chemical potential for SST (see Sec. 5.2), suppose that we apply a potential which is equal to u_1 in the subsystem with volume V_1 and is equal to u_2 in that with volume V_2 . Since the addition of a uniform potential u simply changes the free energy $F(T; V, N)$ to $F(T; V, N) + uN$, the variational relation in this case becomes

$$\begin{aligned} & F(T; V_1, N_1) + u_1 N_1 + F(T; V_2, N_2) + u_2 N_2 \\ &= \min_{\substack{N'_1, N'_2 \\ (N'_1 + N'_2 = N)}} \{F(T; V_1, N'_1) + u_1 N'_1 + F(T; V_2, N'_2) + u_2 N'_2\}. \end{aligned} \quad (2.13)$$

Then the corresponding balance condition becomes

$$\mu(T; V_1, N_1) + u_1 = \mu(T; V_2, N_2) + u_2 \quad (2.14)$$

which clearly shows that $\mu(T; V, N)$ is a kind of potential.¹⁶

These examples illustrate a very important role played by intensive quantities in thermodynamics, which role will be crucial to our construction of SST. Suppose

¹⁵ More precisely, the free energy is defined so that to ensure this coincidence.

¹⁶ Note that $\mu(T; V, N)$ is here defined by (2.12). It is also useful to consider the “electrochemical potential” $\tilde{\mu}_u(T; V, N) = \mu(T; V, N) + u$, but we do not use it here.

in general that one has an extensive variable (V or N in the present case) in the parameterization of states. Also suppose that two states are in touch with each other, and each of them are allowed to change this extensive variable under the constraint (like $V'_1 + V'_2 = V$ or $N'_1 + N'_2 = N$) that the sum of the extensive variables is fixed. Then there exists an intensive quantity (like p or μ) which is *conjugate* to the extensive variable in question, and the condition for the two states to balance with each other is represented by the equality (like (2.9) or (2.11)) of the intensive quantity. The product of the original extensive variable and the conjugate intensive variable always has the dimension of energy.

Finally we write down some of the useful relations which involve the pressure and the chemical potential. From the extensivity (2.4) of the free energy, one gets the Euler equation

$$F(T; V, N) = -V p(T; V, N) + N \mu(T; V, N). \quad (2.15)$$

From the definitions (2.8) and (2.12), one gets

$$\frac{\partial p(T; V, N)}{\partial N} = -\frac{\partial \mu(T; V, N)}{\partial V}, \quad (2.16)$$

which is one of the Maxwell relations. Since the pressure and the chemical potential are intensive,¹⁷ one may define $p(T, \rho) = p(T; 1, N/V) = p(T; V, N)$ and $\mu(T, \rho) = \mu(T; 1, N/V) = \mu(T; V, N)$ with $\rho = N/V$. Then the Maxwell relation (2.16) becomes

$$\frac{\partial p(T, \rho)}{\partial \rho} = \rho \frac{\partial \mu(T, \rho)}{\partial \rho}. \quad (2.17)$$

2.2. Statistical Mechanics

Suppose that we are able to describe a macroscopic physical system using a microscopic dynamics.¹⁸ Let \mathcal{S} be the set of all possible microscopic states of the system. For simplicity we assume that \mathcal{S} is a finite set. The system is characterized by the Hamiltonian $H(\cdot)$, which is a real valued function on \mathcal{S} . For a state $s \in \mathcal{S}$, $H(s)$ represents its energy.

The essential assertion of equilibrium statistical mechanics is that macroscopic properties of an equilibrium state can be reproduced by certain probabilistic models. An important example of such probabilistic models is the *canonical dis-*

¹⁷ $p(T; \lambda V, \lambda N) = p(T; V, N)$ and $\mu(T; \lambda V, \lambda N) = \mu(T; V, N)$ for any $\lambda > 0$.

¹⁸ The description may not be ultimately microscopic. A necessary requirement is that one can write down a reasonable microscopic Hamiltonian.

tribution in which the probability of finding the system in a state $s \in \mathcal{S}$ is given by

$$p_{\text{eq}}(s) = \frac{e^{-\beta H(s)}}{Z(\beta)}, \quad (2.18)$$

where $\beta = (k_B T)^{-1}$ is the inverse temperature, and

$$Z(\beta) = \sum_{s \in \mathcal{S}} e^{-\beta H(s)} \quad (2.19)$$

is the partition function. Moreover if we define the free energy as

$$F(\beta) = -\frac{1}{\beta} \log Z(\beta), \quad (2.20)$$

it satisfies all the static properties of the free energy in thermodynamics, including the convexity, and the variation properties.

The formula (2.6) about density fluctuation holds automatically in the canonical formalism. Let us see the derivation. Consider a system describing a fluid, and denote by \mathcal{S}_N the state space when there are N molecules in the system. We define $Z_N(\beta) = \sum_{s \in \mathcal{S}_N} e^{-\beta H(s)}$ and $F(\beta, N) = -(1/\beta) \log Z_N(\beta)$. Consider a new system obtained by weakly coupling two identical copies of the above system, and suppose that the total number of molecules is fixed to $2N$. Then the probability of finding a pair of states (s, s') with $s \in \mathcal{S}_{N_1}$, $s' \in \mathcal{S}_{N_2}$, and $N_1 + N_2 = 2N$ is

$$p_{\text{eq}}(s, s') = \frac{e^{-\beta\{H(s)+H(s')\}}}{Z_{\text{tot}}(\beta)}, \quad (2.21)$$

where $Z_{\text{tot}}(\beta)$ is the partition function of the whole system. Then the probability $\tilde{p}(N_1, N_2)$ of finding N_1 and N_2 molecules in the first and the second systems, respectively, is

$$\begin{aligned} \tilde{p}(N_1, N_2) &= \sum_{\substack{s \in \mathcal{S}_{N_1} \\ s' \in \mathcal{S}_{N_2}}} p_{\text{eq}}(s, s') \\ &= \frac{Z_{N_1}(\beta) Z_{N_2}(\beta)}{Z_{\text{tot}}(\beta)} \\ &= \exp[-\beta\{F(\beta, N_1) + F(\beta, N_2) - F_{\text{tot}}(\beta)\}], \end{aligned} \quad (2.22)$$

which is nothing but the desired formula (2.6).

2.3. Markov Processes

Although statistical mechanics reproduces static aspects of thermodynamics, it does not deal with dynamic properties such as the approach to equilibrium and the second law. To investigate these points from microscopic (deterministic)

dynamics is indeed a very difficult problem, whose understanding is still poor. For some of the known results, see, for example. Refs. 77–79). If we become less ambitious and start from effective stochastic models, then we have rather satisfactory understanding of these points.

2.3.1. Definition of a General Markov Process

Again let \mathcal{S} be the set of all microscopic states in a physical system. A Markov process on \mathcal{S} is defined by specifying transition rates $c(s \rightarrow s') \geq 0$ for all $s \neq s' \in \mathcal{S}$. The transition rate $c(s \rightarrow s')$ is the rate (i.e., the probability divided by the time span) that the system changes its state from s to s' .

Let $p_t(s)$ be the probability distribution at time t . Then its time evolution is governed by the *master equation*,

$$\frac{d}{dt} p_t(s) = \sum_{\substack{s' \in \mathcal{S} \\ (s' \neq s)}} \{-c(s \rightarrow s') p_t(s) + c(s' \rightarrow s) p_t(s')\}, \quad (2.23)$$

for any $s \in \mathcal{S}$.

A Markov process is said to be *ergodic* if all the states are “connected” by nonvanishing transition rates.¹⁹ In an ergodic Markov process, it is known that the probability distribution $p_t(s)$ with an arbitrary initial condition converges to a unique stationary distribution $p_\infty(s) > 0$. Then from the master Eq. (2.23), one finds that the stationary distribution is characterized by the equation

$$\sum_{\substack{s' \in \mathcal{S} \\ (s' \neq s)}} \{-c(s \rightarrow s') p_\infty(s) + c(s' \rightarrow s) p_\infty(s')\} = 0, \quad (2.24)$$

for any $s \in \mathcal{S}$. See, for example Ref. 80.

2.3.2. Detailed Balance Condition

The convergence to a unique stationary distribution suggests that, if one wishes to model a dynamics around equilibrium, one should build a model so that the stationary distribution $p_\infty(s)$ coincides with the canonical distribution $p_{\text{eq}}(s)$ of (2.18). A sufficient (but far from being necessary) condition for this to be the case is that the transition rates satisfy

$$c(s \rightarrow s') p_{\text{eq}}(s) = c(s' \rightarrow s) p_{\text{eq}}(s') \quad (2.25)$$

¹⁹ More precisely, for any $s, s' \in \mathcal{S}$, one can find a finite sequence $s_1, s_2, \dots, s_n \in \mathcal{S}$ such that $s_1 = s$, $s_n = s'$, and $c(s_j \rightarrow s_{j+1}) \neq 0$ for any $j = 1, 2, \dots, n - 1$.

for an arbitrary pair $s \neq s' \in \mathcal{S}$. By substituting (2.25) into (2.24), one finds that each summand vanishes and (2.24) is indeed satisfied with $p_\infty(s) = p_{\text{eq}}(s)$. The equality (2.25) is called the *detailed balance condition* with respect to the distribution $p_{\text{eq}}(s)$.

Today one always assumes the detailed balance condition (2.25) when studying dynamics around equilibrium using a Markov process. This convention is based on a deep reason, which was originally pointed out by Onsager,^(7,8) that such models automatically satisfy macroscopic symmetry known as “reciprocity.” See Sec. 1.3.1.

By substituting the formula (2.18) of the canonical distribution into the condition (2.25), it is rewritten as

$$\frac{c(s \rightarrow s')}{c(s' \rightarrow s)} = \exp[\beta\{H(s) - H(s')\}], \quad (2.26)$$

for any $s \neq s'$ such that $c(s \rightarrow s') \neq 0$. Usually the condition (2.26) is also called the detailed balance condition. A standard example of transition rates satisfying (2.26) is

$$c(s \rightarrow s') = a(s, s') \phi(\beta\{H(s') - H(s)\}), \quad (2.27)$$

where $a(s, s') = a(s', s) \geq 0$ are arbitrary weights which ensure the ergodicity,²⁰ and $\phi(h)$ is a function which satisfies

$$\phi(h) = e^{-h} \phi(-h), \quad (2.28)$$

for any h . The standard choices of $\phi(h)$ are i) the *exponential rule* with $\phi(h) = e^{-h/2}$, ii) the *heat bath (or Kawasaki) rule* with $\phi(h) = (1 + e^h)^{-1}$, and iii) the *Metropolis rule* with $\phi(h) = 1$ if $h \leq 0$ and $\phi(h) = e^{-h}$ if $h \geq 0$. In equilibrium dynamics, these (and other) rules can be used rather arbitrarily depending on one’s taste. But it has been realized these days^(44,81) that the choice of rule crucially modifies the nature of the stationary state if one considers nonequilibrium dynamics. Indeed we will see a drastic example in Sec. B.8 in the Appendix.

2.3.3. The Second Law

To study the minimum work principle (2.5), we must theoretically formulate mechanical operations by an outside agent. When the agent moves a wall of the container, she is essentially changing the potential energy profile for the fluid molecules. We therefore consider a Hamiltonian $H^{(\alpha)}(s)$ with an additional control parameter α , and let $c^{(\alpha)}(s \rightarrow s')$ be transition rates whose stationary distribution

²⁰ A simple choice is to set $a(s, s') = 1$ if s' can be “directly reached” from s , and $a(s, s') = 0$ otherwise.

is the canonical distribution²¹

$$p_{\text{eq}}^{(\alpha)}(s) = \frac{1}{Z^{(\alpha)}(\beta)} \exp[-\beta H^{(\alpha)}(s)]. \quad (2.29)$$

Suppose that the agent changes this parameter according to a prefixed (arbitrary) function²² $\alpha(t)$ with $0 \leq t \leq t_f$. (t_f is the time at which the operation ends.) Since the Hamiltonian $H^{(\alpha(t))}(s)$ is now time-dependent, the transition rates $c^{(\alpha(t))}(s \rightarrow s')$ also become time-dependent.

To mimic the situation in thermodynamics, we assume that, at time $t = 0$, the probability distribution coincides with the equilibrium state for $\alpha = \alpha(0)$, i.e., we set $p_0(s) = p_{\text{eq}}^{(\alpha(0))}(s)$. The probability distribution $p_t(s)$ for $0 \leq t \leq t_f$ is the solution of the time-dependent master equation

$$\frac{d}{dt} p_t(s) = \sum_{\substack{s' \in \mathcal{S} \\ (s' \neq s)}} \{ -c^{(\alpha(t))}(s \rightarrow s') p_t(s) + c^{(\alpha(t))}(s' \rightarrow s) p_t(s') \}, \quad (2.30)$$

which is simply obtained by substituting the time-dependent transition rates into the master Eq. (2.23). Let us denote the average over the distribution $p_t(s)$ as

$$\langle g(s) \rangle_t = \sum_{s \in \mathcal{S}} g(s) p_t(s), \quad (2.31)$$

where $g(s)$ is an arbitrary function on \mathcal{S} .

Now, in a general time-dependent Markov process, a theorem sometimes called the “second law” is known²³ such a theorem was first proved by Yosida. See XIII-3 of Ref. 83. We shall describe it carefully in the Appendix C. The theorem readily applies to the present situation, where the key quantity defined in (C.2) becomes

$$\varphi^{(\alpha)}(s) = -\log p_{\text{eq}}^{(\alpha)}(s) = \beta \{ H^{(\alpha)}(s) - F(\beta, \alpha) \}, \quad (2.32)$$

with

$$F(\beta, \alpha) = -\frac{1}{\beta} \log \sum_{s \in \mathcal{S}} \exp [-\beta H^{(\alpha)}(s)] \quad (2.33)$$

²¹ As an example, one replaces $H(s)$ in (2.27) with $H^{(\alpha)}(s)$.

²² Here we are not including any feedback from the system to the agent. (The agent does what she has decided to do, whatever the reaction of the system is.) To include the effects of feedback seems to be a highly nontrivial problem.

²³ According to Ref. 82.

being the free energy with the parameter α . Then the basic inequality (C.5) implies that, for any differentiable function $\alpha(t)$, one has

$$\int_0^{t_f} dt \frac{d\alpha(t)}{dt} \left\langle \frac{d}{d\alpha} H_\alpha(s) \Big|_{\alpha=\alpha(t)} \right\rangle_t \geq F(\beta, \alpha(t_f)) - F(\beta, \alpha(0)). \quad (2.34)$$

Let us claim that the left-hand side of (2.34) is precisely the total mechanical work done by the external agent. Consider a change from time t to $t + \Delta t$, where Δt is small. The change of the Hamiltonian is $\Delta H(s) = H^{\alpha(t+\Delta t)}(s) - H^{\alpha(t)}(s)$. Since the agent directly modifies the Hamiltonian, the work done by the agent between t and $t + \Delta t$ is equal to²⁴ $\langle \Delta H(s) \rangle_t + O((\Delta t)^2)$. By summing this up (and letting $\Delta t \rightarrow 0$), we get the left-hand side of (2.34). With this interpretation, the general inequality (2.34) is nothing but the minimum work principle (2.5).

3. NOEQUILIBRIUM STEADY STATES AND LOCAL STEADY STATES

Equilibrium thermodynamics, equilibrium statistical mechanics, and Markov process description of equilibrium dynamics, which we reviewed briefly in Sec. 2 are *universal* theoretical frameworks that apply to equilibrium states of arbitrary macroscopic physical systems. As we have discussed in Sec. 1.1, our goal in the present paper is to construct such a universal thermodynamics that applies to nonequilibrium steady states.

In the present section, we shall make clear the class of systems that we study, and describe their nonequilibrium steady states (Sec. 3.1). We then discuss the important notion of *local steady state* (Sec. 3.2).

3.1. Nonequilibrium Steady States

A macroscopic physical system is in a *nonequilibrium steady state* if it shows no macroscopically observable changes while constantly exchanging energy with the environment.

Although our aim is to construct a universally applicable theory, it is useful (or even necessary) to work in concrete settings. Let us describe typical examples that we shall study in the present paper.

3.1.1. Heat Conduction

The first example is heat conduction in a fluid. Suppose that a fluid consisting of a single substance is contained in a cylindrical container as in Fig. 4. The upper

²⁴Note that this is different from $\langle H^{\alpha(t+\Delta t)}(s) \rangle_{t+\Delta t} - \langle H^{\alpha(t)}(s) \rangle_t$. The difference is nothing but the energy exchanged as “heat.”

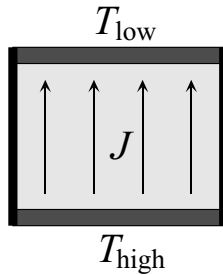


Fig. 4. The upper and the lower walls have temperatures T_{low} and T_{high} , respectively. In the nonequilibrium steady state, the fluid in the container carries a steady heat current in the vertical direction. We assume that there is no convection.

and the lower walls of the cylinder are kept at constant temperatures T_{low} and T_{high} , respectively, with the aid of external heat baths. The side walls of the container are perfectly adiabatic.

If the system is kept in this setting for a sufficiently long time, it will finally reach a steady state without any macroscopically observable changes. We assume that convection does not take place, so there is no net flow in the fluid. But there is a constant heat current from the lower wall to the upper wall, which constantly carries energy from one heat bath to the other. This is a typical nonequilibrium steady state.

3.1.2. Shear Flow

The second example is a fluid under shear. Consider a fluid in a box shaped container whose upper and lower walls are made of a “sticky” material. The upper

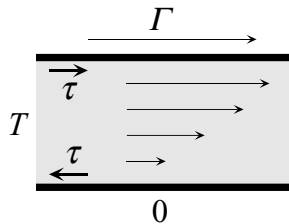


Fig. 5. There is a fluid between two “sticky” horizontal walls. The upper wall moves with a constant speed Γ while the lower wall is at rest. In the nonequilibrium steady state, the fluid develops a velocity gradient. The forces that the upper and the lower walls exert on fluid are exactly opposite with each other.

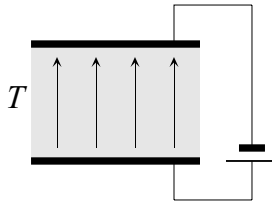


Fig. 6. An electrically conducting fluid attached to a heat bath is put in a uniform electric field. In a steady state one has a constant electric current. Joule heat generated in the fluid is absorbed by the heat bath.

wall moves with a constant speed Γ while the lower wall is at rest.²⁵ We assume that the fluid is in touch with a heat bath at constant temperature T . Since the moving wall does a positive work on the fluid, the fluid must constantly throw energy away to the bath in order not to heat up.

If we keep the system in this setting for a sufficiently long time, it finally reaches a steady state in which the fluid moves horizontally with varying speeds as in Fig. 5. The wall constantly injects energy into the system as a mechanical work while the fluid releases energy to the heat bath. This is another typical nonequilibrium steady state.

Since the fluid gets no acceleration in a steady state, the total force exerted on the whole fluid must be vanishing. This means that the forces that the upper and the lower walls exert on the fluid are exactly opposite with each other. The same argument, when applied to an arbitrary region in the fluid, leads to the well-known fact that the shear stress, defined as the flux of horizontal momentum in the vertical direction, is constant everywhere in the sheared fluid.

3.1.3. Electrical Conduction in a Fluid

The third example is electrical conduction in a fluid as in Fig. 6. When a constant electric field is applied to a conducting fluid which is in touch with a heat bath at a constant temperature, there appears a steady electric current. It should be noted that the electric field does not generate particle flow in the fluid, but only generates a flow of electric carriers.²⁶ Since a normal conductor always generates Joule heat, there is a constant flow of energy to the heat bath. This is also a typical nonequilibrium steady state.

²⁵ One should devise a proper geometry (periodic boundary conditions) to make it possible for the upper wall to keep on moving.

²⁶ There must be a mechanism to move the carrier from one plate to the other so that to maintain a steady current. When the carrier is electron, this is simply done by using a battery as in Fig. 6.

3.2. Local Steady State

Let us discuss the notion of *local steady state* which is central to our study.

To be concrete let us concentrate on the case of heat conduction in a fluid (Sec. 3.1.1). In general the local temperature and the local density of the fluid vary continuously as functions of the position.²⁷ If one looks at a sufficiently small portion of the fluid, however, both the temperature T and the density ρ are essentially constants.

In the standard treatment of weakly nonequilibrium systems (see Sec. 1.3.1), one assumes that the state within the small portion can be regarded as the equilibrium state with the same T and ρ . Then the whole nonequilibrium state with varying temperature and density is constructed by “patching” together these *local steady states*.

In general situations where the system is not necessarily close to equilibrium, however, this treatment is not sufficient. No matter how small the portion may be, there always exists a finite heat flux going through it. Therefore the local state in this small portion cannot be isotropic. Since equilibrium states are always isotropic in a fluid, this means that the local state cannot be treated as a local equilibrium state. It should be treated rather as a *local steady state*.

A local steady state is in general anisotropic. It is characterized by the temperature T , the density ρ , and (at least) one additional parameter (which we do not yet specify) which measures the “degree of nonequilibrium.” Macroscopic quantities of the heat conducting fluid, such as the pressure, viscosity, and heat conductivity, should in principle depend not only on T and ρ but also on the additional nonequilibrium parameter. The main goal of our work is to present a thermodynamics that applies to local steady states.²⁸

3.3. Realization of Local Steady States

As a next step we discuss how one can realize local steady states in each of the concrete examples.

3.3.1. Heat Conduction

Consider again heat conduction in a fluid. Suppose that the system has a nice symmetry and we get a steady state which is transitionally invariant in the

²⁷ Although the density is defined unambiguously in any situation, the definition of temperature is much more delicate. Here we simply assume that the local temperature can be measured by a small thermometer. We will discuss more about the definition of temperature in Sec. 8.3.1.

²⁸ As a next step, one wishes to see how these local steady states can be “patched” together to form a global nonequilibrium steady state. We hope this will be a topic of our future works.

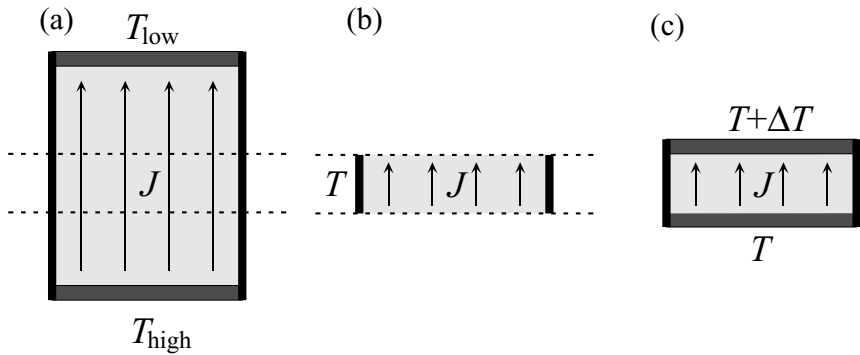


Fig. 7. Local steady state for heat conduction. (a) There is a temperature gradient and heat flux in the vertical direction. (b) If one concentrates on a thin region of the system, the temperature T and the density are essentially constant. This is a local steady state. (c) We further assume that the same local steady state can be realized in a thin system by adjusting the temperature of the upper and the lower walls.

horizontal directions. The heat flux flows in the vertical direction as in Fig. 7(a). We let the heat flux J be the total amount of heat that passes through an arbitrary horizontal plane in the fluid within a unit time. Note that the heat flux J is independent of the choice of the plane because of the energy conservation.

Take a region in the fluid in between two (fictitious) horizontal planes. If the width of the region is sufficiently small, the temperature and the density in the region may be regarded as constant. This thin system realizes a local steady state for heat conduction as in Fig. 7(b).

Suppose that one inserts into the fluid a horizontal wall with very efficient thermal conductivity and negligible thickness. Since there is no macroscopic flow of fluid to begin with, and the temperature is constant on any horizontal plane, it is expected that the insertion of the wall does not cause any macroscopically observable changes.²⁹ Then one can replace the two (fictitious) planes that determine the thin region with two conducting horizontal walls without making any macroscopic changes. Moreover, by connecting the two walls to heat baths with precise temperatures, one can “cut out” the thin region from the rest of the system as in Fig. 7(c). In this manner we can realize a local steady state in an isolated form.

²⁹ This statement is not as obvious as it first seems. In reality there often appears a seemingly discontinuous temperature jump between a fluid and a wall. Our assumption relies on an expectation that this jump can be made negligibly small by using a wall made of a suitable material with a suitable surface condition.

3.3.2. Shear Flow

In the case of sheared fluid (Sec. 3.1.2) identification of a local steady state is (at least conceptually) much easier. If the contact with the heat bath is efficient enough, one may regard that the whole system has a uniform temperature. If this is the case, the state of the whole system is itself a local steady state.

When the temperature difference within the fluid is not negligible, one may again focus on a thin region to get a local steady state. The technique of inserting thin walls can be used in this situation as well. We here use a sticky wall with a negligible width and insert it horizontally in such a way that it has precisely the same velocity as the fluid around it. We can then isolate a local steady state.³⁰

3.3.3. Electrical Conduction in a Fluid

The case of electrical conduction in a fluid (Sec. 3.1.3) can be treated in a similar manner as the previous two examples. If there are variations in the temperature or the density, we again restrict ourselves to a thin horizontal region to get a local steady state. When electrons carry current, an electrically conducting thin wall with a precisely fixed electric potential may be inserted to the fluid without changing macroscopic behavior.

4. BASIC FRAMEWORK OF STEADY STATE THERMODYNAMICS

As a first step of the construction of steady state thermodynamics (SST), we carefully examine basic operations to local steady states (Sec. 4.1). Then we discuss how we should choose nonequilibrium thermodynamic variables (Sec. 4.2). To make the discussions concrete, we first restrict ourselves to the case of heat conduction. Other cases are treated separately (Secs. 4.3 and 4.4).

4.1. Operations to Local Steady States

As we saw in Sec. 2.1, various operations (i.e., decomposition, combination, and scaling) on equilibrium states are essential building blocks of equilibrium thermodynamics. We shall now examine how these operations should be generalized to nonequilibrium steady states. This is not at all a trivial task since nonequilibrium steady states are inevitably anisotropic, and there is a steady flow of energy going through it.

³⁰When there is a temperature gradient, one gets a local steady state with a heat current as well as a shear. We here assume that the latter has a dominant effect.

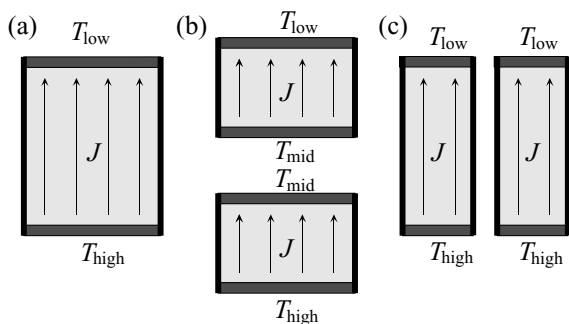


Fig. 8. Two possible ways (b), (c) to decompose a heat conducting steady state (a). Both the ways are theoretically sensible.

We examine the case of steady heat conduction in a fluid. In order to find general structures of steady states, we examine a heat conducting state between the temperatures T_{low} and T_{high} (Fig. 8(a)). We still do not take the limit of local steady states.

There are two natural (and theoretical sensible) ways of decomposing the steady state. In the first way, one inserts a thin horizontal wall with efficient heat conduction as in Sec. 3.3.1. Then one measures the temperature of the wall (which we call T_{mid}) and attach the wall to a heat bath with the same temperature T_{mid} . We expect that these procedures do not cause any macroscopically observable changes. Finally one splits the middle wall into two, and gets the situation in Fig. 8(b), where one has two steady states. In the second way, which is much more straightforward, one simply inserts a thin adiabatic wall vertically to split the system into two as in Fig. 8(c). One can of course revert these procedures, and combine the two states to get the original one.

We next examine how one should combine two heat conducting states which have different densities (or which contain different kinds of fluids). One natural way is a combination in the vertical direction. We prepare two heat conducting states between T_{low} and T_{mid} and between T_{mid} and T_{high} . The two systems have the same horizontal cross sections. We then attach the two walls with the temperature T_{mid} together as in Fig. 9(a). If the two states have exactly the same heat flux J , there is no heat flow between the middle wall and the heat bath with T_{mid} . This means that we can simply disconnect this heat bath without making any changes to the combined steady states. This way of combining two steady states always works provided that the temperatures at the attached walls are the same (which is T_{mid}) and the heat flux J in the two states are identical with each other. We can regard this as a natural extension of the combination of two states frequently used in equilibrium thermodynamics.

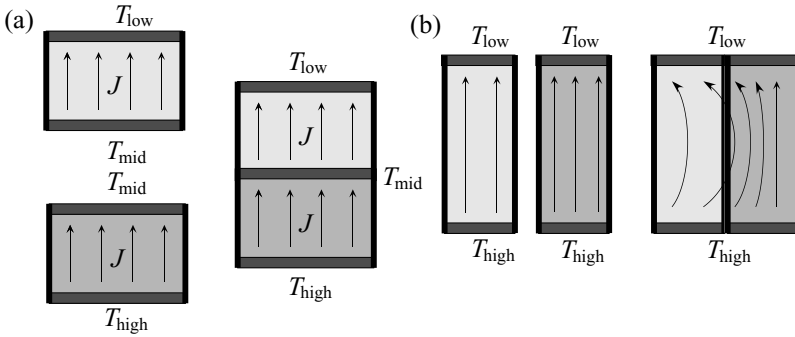


Fig. 9. Two possible ways of combining two heat conducting states which have different densities. (a) Contact through a horizontal wall does not change the two states as long as the temperatures at the attached walls (denoted as T_{mid}) coincide and the heat flux J in the two states are identical. (b) Contact through a conducting vertical wall may inevitably lead to a modification of the heat flow pattern. We are therefore led to consider only the vertical combination/decomposition scheme (a).

As in the decomposition scheme, we can also think about combinations in the horizontal direction. We can put two heat conducting states together along a vertical heat conducting wall as in Fig. 9(b). This combination scheme too may look reasonable at first glance. But note that the contact always modifies the heat flux pattern unless the vertical temperature profiles of the two states before the contact are exactly identical. Since two different fluids (or fluid in two different densities) generally develop different (nonlinear) temperature profiles, we must conclude that in general this horizontal contact modifies the two states. It therefore cannot be used as a combination scheme in thermodynamics.³¹

In conclusion, the decomposition/combination in the vertical direction (in which one separates a system, or puts two systems together along a horizontal plane) works in any situation, while that in the horizontal direction is less robust. The advantage of the former scheme is that it relies only on a conservation law that is independent of thermodynamics. More precisely the constancy of the heat flux J is guaranteed by the energy conservation law and the steadiness of the states. We are therefore led to a conclusion that, in nonequilibrium steady states for heat conduction, the decomposition and combination of states should be done in the

³¹ If the temperature profiles are always linear, then one can say that the two profiles with the same terminal temperatures are identical. One might think this is always the case in local steady states realized in very thin systems. But we point out that, no matter how thin a system may be, there can be a phase coexistence in it, which leads to a nonlinear temperature profile. Therefore the horizontal combination scheme in heat conduction may be useful only when one (i) restricts oneself to local steady states, and (ii) rules out the possibility of phase coexistence. We still do not know if we can construct a meaningful thermodynamics starting from this observation.

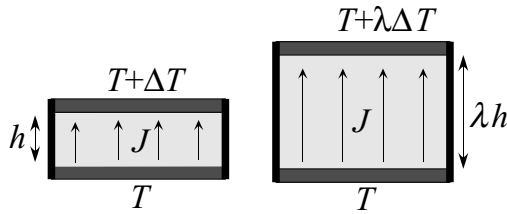


Fig. 10. Scaling in a local steady state of a heat conducting fluid. We fix the horizontal cross section and scale only in the vertical direction by a factor $\lambda > 0$. The height h (and hence the volume), the amount of substance N , and the (small) temperature difference ΔT are scaled by λ , while the temperature T and the heat flux J are unchanged.

vertical direction using horizontal planes, keeping the horizontal cross section constant. See, again, Figs. 8(b) and 9(a).

For a local steady state, which is defined on a sufficiently thin system, one can define a scaling operation. Following the decomposition/combination scheme, we shall fix the cross section of the system and scale only in the vertical direction.³² When doing this we must carefully choose the (small) temperature difference so that the heat flux J is kept constant. See Fig. 10.

4.2. Choice of Nonequilibrium Variables

We now turn to the problem of describing local steady states in a qualitative manner. The main issue here is how one should choose a new thermodynamic variable representing the “degree of nonequilibrium.” Rather surprisingly, we will see that, by assuming that a reasonable thermodynamics exists, we can determine the nonequilibrium variable almost uniquely.

Let us again use the heat conduction as an example, and take a sufficiently thin system to realize a local steady state. To characterize the local steady state, we definitely need the temperature T , the volume V , and the amount of substance N . Note that we only need a single temperature T since a local steady state has an essentially constant temperature. In addition to these three variables, we need a “nonequilibrium variable” as we discussed in Sec. 3.2.

When choosing the nonequilibrium variable, we first postulate that the variable should correspond to a physically “natural” quantity. Then, in a local steady state for heat conduction, there are essentially two candidates. One is the heat flux J , which is the total energy that passes through any horizontal plane

³² The scaling factor λ should not be too large to keep the state a local steady state.

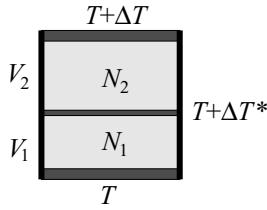


Fig. 11. A local steady state with heat conduction is separated into lower and upper parts (with the volumes and the amounts of fluid equal to V_1, V_2 , and N_1, N_2 , respectively) by a thermally conducting horizontal wall. The temperatures T and $T + \Delta T$ of the lower and the upper walls, respectively, are fixed. We want to determine the temperature $T + \Delta T^*$ at the separating wall.

within a unit time. The other is the temperature difference ΔT between the upper and the lower walls.³³

To see the characters of these nonequilibrium variables, we examine the scaling transformation of the local steady state (Fig. 10). When the system is scaled by a factor $\lambda > 0$ in the vertical direction, the extensive variables V and N are scaled to become λV and λN , respectively, while the intensive variable T is unchanged. The heat flux J is unchanged because we want to keep the local state unchanged. (More formally speaking, it is our convention, which followed almost inevitably from the considerations in Sec. 4.1, to keep J constant when extending the system in the vertical direction.) The temperature difference ΔT , on the other hand, must be scaled to $\lambda \Delta T$ in order to maintain the same heat flux. Therefore, within our convention of scaling, the nonequilibrium variable J acts as an intensive variable while ΔT acts as an extensive variable.

Thus our parameterization of a local steady state can either be³⁴ $(T, J; V, N)$ or $(T; V, N, \Delta T)$. We wish to examine whether we can get consistent thermodynamics by using these parameterizations.

We first argue that a thermodynamics with the parameterization $(T; V, N, \Delta T)$ is inconsistent, or, to say the least, not useful. To demonstrate this we consider the situation in Fig. 11, where a single fluid of volume V is separated into two parts by a horizontal wall. The volumes and the amounts of fluid in the lower and upper parts are fixed to V_1, V_2 , and N_1, N_2 , respectively. The separating wall is thermally conducting. The upper and the lower walls are fixed, and have fixed temperatures $T + \Delta T$ and T , respectively, where $\Delta T \ll T$. The temperature $T + \Delta T^*$ at the separating wall is not fixed, but should be uniquely determined in the steady state.

³³ We have assumed that the temperature in a local steady state is essentially constant. But there must be a nonvanishing temperature difference ΔT to maintain the heat conduction. Of course we have $\Delta T \ll T$.

³⁴ Recall the notation to separate intensive and extensive variables by a semicolon. See Sec. 2.1.1.

Let us note that the situation here is completely analogous to those we have seen in Sec. 2.1.3. (See, in particular, the discussion at the end of the section.) Here the temperature difference in the lower part (i.e., the difference between the temperatures of the lower wall and the separating wall) is $\Delta T_1 = \Delta T^*$, while that in the upper part is $\Delta T_2 = \Delta T - \Delta T^*$. Since ΔT is fixed, their sum $\Delta T_1 + \Delta T_2$ is fixed. Let us assume that the general structure of thermodynamics is maintained here. Then there should be an intensive quantity $\nu(T; V, N, \Delta T)$ which is conjugate to ΔT , and ΔT^* should be determined by the balance condition

$$\nu(T; V_1, N_1, \Delta T^*) = \nu(T; V_2, N_2, \Delta T - \Delta T^*). \quad (4.1)$$

We know, on the other hand, that the balance of heat flux between two subsystems can be universally expressed by the equality

$$J(T; V_1, N_1, \Delta T^*) = J(T; V_2, N_2, \Delta T - \Delta T^*), \quad (4.2)$$

where $J(T; V, N, \Delta T)$ is the heat flux written as a function of T , V , N , and ΔT . Since the two conditions (4.1) and (4.2) should be equivalent for each T , there must be a function $g(J, T)$ such that

$$\nu(T; V, N, \Delta T) = g(J(T; V, N, \Delta T), T), \quad (4.3)$$

for any T , V , N , and ΔT . But note here that the quantity ν (which is conjugate to δT) is dimensionless³⁵ while the heat flux J has the dimension of energy divided by time. This means that the function $g(J, T)$ must include (at least) one universal constant which has the dimension of time.³⁶ But it is quite unlikely (if not impossible) that a theory requires such a new universal constant. We must conclude that a thermodynamics with the parameterization $(T; V, N, \Delta T)$ of local steady states (even if it exists) is highly unnatural.

On the other hand, a thermodynamics with the parameterization $(T, J; V, N)$ does not suffer from such a pathology. Here the “degree of nonequilibrium” is directly taken into account through the intensive variable J , which directly accounts for the energy conservation law. Since the role of an intensive variable in thermodynamics is to set the environment for the system, there is no room for internal inconsistencies to appear.

We are therefore led to the conclusion that *a heat conducting local steady state should be parameterized as $(T, J; V, N)$, where the nonequilibrium variable J is intensive.*³⁷

The general lesson is as follows. To get a sensible thermodynamics, *the “degree of nonequilibrium” should be taken into account through an intensive variable which manifestly represents a conservation law that is imposed by physical*

³⁵ Our convention is that temperature has the dimension of energy.

³⁶ For example, $g(J, T) = t_0 J/T$ is dimensionless when t_0 is a constant with the dimension of time.

³⁷ There is a possibility that a natural thermodynamic variable is a function $\psi(J)$ rather than J itself. See footnote 44 in Sec. 7.3.

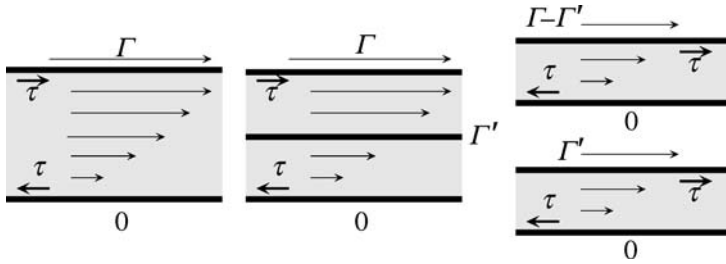


Fig. 12. Decomposition of a steady state of sheared fluid. One inserts a thin horizontal wall with the precise velocity Γ' as in (b). By splitting the two parts and Galilei transforming the upper system, one gets the situation in (c). Note that the shear force τ is preserved in this decomposition. When combining two states, one starts from (c) and goes back to (b).

laws out of thermodynamics. An extensive nonequilibrium variable which looks natural from a physical point of view may not be natural for a thermodynamic theory. This is because the corresponding variational principle may conflict (or may become redundant) with the already existing conservation law.

4.3. Shear Flow

Let us examine how the discussions in Secs. 4.1 and 4.2 should be extended to local steady states of a sheared fluid.

Let us start from the decomposition/combination scheme. If the fluid is two-dimensional (as in Fig. 5), then it is obvious that decomposition and combination must be done in the vertical direction along a horizontal line. Decomposition or combination in other directions are simply impossible because of the horizontal flow. In a three dimensional fluid, one might first imagine that decomposition in other directions³⁸ can be used, but it turns out that it is not possible when there is a phase separation within the system. Anyway it is most natural to stick on a scheme which does not depend on the dimensionality. We shall always decompose or combine systems in the vertical direction, along horizontal planes.

To decompose a steady state, one first inserts a thin sticky wall horizontally in such a way that the velocity of the wall is identical to that of fluid around it. We expect that this insertion does not modify the state macroscopically. Then one decomposes the inserted wall into two, and splits the system into two parts. Note that the shear force τ is preserved in this process. If one wishes to bring both the states into the standard form (where the lower wall is at rest), one performs a Galilei transformation to the upper system as in Fig. 12.

³⁸ For example one can think about cutting the system into two along a plane parallel to the page.

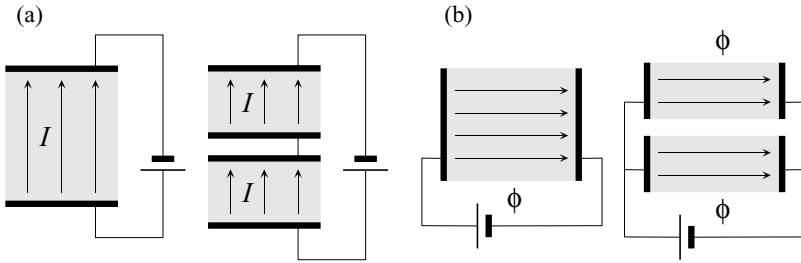


Fig. 13. Two possible schemes of decomposition/combination in a steady state of fluid with electric current. (a) The first scheme is the same as that for heat conduction if we replace the heat flux J with the total electric current I . The charge conservation law ensures that the total current I is a “good” intensive nonequilibrium variable. (b) The second scheme makes use of the fact that the electric potential difference ϕ is constant when one splits or combines systems along a plane parallel to the current. Then ϕ becomes the intensive nonequilibrium variable.

When one combines two states into one, one first prepares two steady states (as in Fig. 12(c)) with the identical shear force τ , and then combine them (after a Galilei transformation) as in Fig. 12(b).

It is then obvious that the shear velocity Γ (which is the difference between the velocities of the upper and the lower walls) is the extensive variable, and the shear force τ is the intensive variable. From an argument parallel to that in Sec. 4.2, we find that a thermodynamics with the parameterization $(T; V, N, \Gamma)$ is inappropriate. We shall parameterize local steady states as $(T, \tau; V, N)$, and look for a useful thermodynamics.

4.4. Electrical Conduction in a Fluid

Treatment of steady states in an electrically conducting fluid is somewhat more delicate than the other two examples. It seems that, in some situations, there are *two* completely different formulations of thermodynamics, whose relations are far from obvious (and not yet clear to us).

Obviously it is possible to develop a scheme completely parallel to that for heat conduction. For this, one simply identifies the total electric current I with the heat flux J . Then one decomposes, combines, and scales local steady states in the direction of the current as in Fig. 13(a). In the corresponding thermodynamics, the total electric current I becomes the intensive nonequilibrium variable. Local steady states are parameterized as $(T, I; V, N)$.

But this is not the only possible thermodynamics. If one can neglect the effect of charge screening at the walls, then the difference ϕ in the electric potential between the two walls is constant. The potential ϕ is unchanged if one decomposes the system along a plane parallel to the electric current as in

Fig. 13(b). We can use the corresponding combination and scaling convention to construct a thermodynamics, where the electric potential difference ϕ becomes the nonequilibrium intensive variable. Local steady states are parameterized as $(T, \phi; V, N)$.

It is quite interesting that there are two different formulations of thermodynamics for a single physical system. The two are truly different theories since they are based on different schemes of scaling. One must note that the two possible theories can never be related with each other simply, for example, by a Legendre transformation.

It is an intriguing problem to find the true meaning of the (apparent) possibility of the two formulations of thermodynamics. In particular it is exciting to find an “unifying” theory which includes the physics of both the theories, provided that both the theories are found to be physically meaningful.³⁹

5. OPERATIONAL DETERMINATION OF THERMODYNAMIC QUANTITIES

In Sec. 4, we have determined the basic structure of steady state thermodynamics (SST), assuming that a sensible thermodynamics for local steady states does exist. We now turn to the task of determining thermodynamic quantities. In doing so, we insist on defining everything through operational procedures which are (at least in principle) experimentally realizable.

In the present section, we discuss how one can determine the pressure (Sec. 5.1) and the chemical potential (Sec. 5.2) of a local steady state $(T, \nu; V, N)$, and further show that these quantities satisfy the Maxwell relation (Sec. 5.3). Here the variable ν represents a general nonequilibrium intensive variable, and should be read as $J, \tau, I,$ or ϕ depending on the model that one has in mind. Although the pressure $p(T, \nu; V, N)$ is fully determined, we here determine only the V, N dependence of the chemical potential $\mu(T, \nu; V, N)$. Determination of T, ν dependence will be discussed later in Sec. 7.2.

The construction in the present section is fairly general and does not depend on specific systems. The convention is that when we say “vertical” direction, it means the direction to which we scale our systems. The reader should simply have in mind, for examples, Figs. 10, 12, and 13, and interpret the word “vertical” in the ordinary sense. Recall that we can think about two different formulations of thermodynamics for electric conduction in a fluid (Sec. 4.4).

³⁹ A less interesting possibility is that only one of the two is physically meaningful. (And much less interesting possibility is that none of them are.)

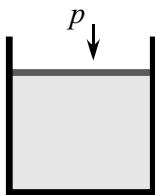


Fig. 14. To be consistent with our convention of scaling, we measure the (mechanical) pressure in the vertical direction and identify it as the SST pressure $p(T, v; V, N)$.

5.1. Pressure-A Mechanical Definition

Pressure is a special thermodynamic quantity, which also has a purely mechanical characterization.⁴⁰

As usual the pressure of a local steady state is defined as the mechanical pressure or through the work needed to make a small change of volume. The only point we have to be careful about is that a nonequilibrium steady state is anisotropic. Since it is our convention to perform decomposition, combination, and scaling only in the vertical direction, we shall only speak about the pressure in the vertical direction. It is obtained as the mechanical pressure exerted on the horizontal walls, or through the relation $\Delta W = p \Delta V$ where ΔW is the mechanical work needed to make a small volume change ΔV by moving a horizontal wall vertically. See Fig. 14.

We denote the pressure thus determined as $p(T, v; V, N)$. Since the vertical force should not change when one scales the system in the vertical direction, we have the intensivity

$$p(T, v; \lambda V, \lambda N) = p(T, v; V, N), \quad (5.1)$$

for any $\lambda > 0$ (which is small enough to maintain local steadiness). Note that in the case of electrical conduction in a fluid, two pressures $p(T, I; V, N)$ and $p(T, \phi; V, N)$ corresponding to the two different formulations of thermodynamics are in general different.

As in equilibrium, we expect the pressure $p(T, v; V, N)$ to be nonincreasing in V . Otherwise a small fluctuation in the volume may be magnified, leading to a catastrophic volume change.

⁴⁰ We can say that equilibrium thermodynamics establishes quantitative connection with mechanics through the pressure and the internal energy. In our construction of SST, we make use of the pressure. But it is extremely difficult (if not impossible) to introduce the notion of internal energy to nonequilibrium steady states since there always is a constant flow of energy. Oono and Paniconi⁽²⁾ indeed tried to define internal energy of SST by extending the notion of adiabaticity. In our construction, we do not make use of adiabaticity.

5.2. Potential Variation Method and Chemical Potential

In contrast to the pressure, the chemical potential is a purely thermodynamic quantity. Therefore to define it for local steady states is a highly nontrivial problem. In the present section, we introduce the *method of potential variation*, which enables one to determine the difference in the chemical potential unambiguously. By using this method, we determine V , N dependence of the chemical potential in a purely operational manner. To our knowledge this method of determining chemical potential was first pointed out and used by Hayashi and Sasa.⁽⁴⁷⁾

Fix the temperature T and the nonequilibrium variable v . We denote by $\mu(\rho) = \mu(T, v; V, N)$ the chemical potential as a function of the density $\rho = N/V$. We have assumed the intensivity

$$\mu(T, v; \lambda V, \lambda N) = \mu(T, v; V, N), \quad (5.2)$$

for any $\lambda > 0$.

Now we apply an external potential which generates a force⁴¹ acting on fluid particles. The potential is equal to a constant u_1 in the lower half of the system, and is equal to u_2 in the upper half. We assume that the potential varies smoothly in the vertical direction between the two regions.

Let the system relax to its steady state under the applied potential. We denote by ρ_1 and ρ_2 the densities of the fluid in the lower and the upper regions, respectively. Since the two regions can freely exchange fluid molecules and are in steady balance with each other, the chemical potential $\mu(\rho)$ (if exists) should satisfy the balance relation

$$\mu(\rho_1) + u_1 = \mu(\rho_2) + u_2, \quad (5.3)$$

which is nothing but the nonequilibrium counterpart of the relation (2.14) in equilibrium thermodynamics. Note that we are again speaking only about contacts of two regions in the vertical direction. As in the definition of the pressure, all the notions should be consistent with our convention of scaling.

To be more logical, we are here defining the chemical potential $\mu(\rho)$ as a quantity that satisfies the condition (5.3), under the assumption that (5.3) for various u_1 and u_2 lead consistently to a function $\mu(\rho)$.

It seems obvious that $\rho_1 \geq \rho_2$ when $u_1 \leq u_2$, since the fluid feels a downward force in the boundary of the two regions. Then (5.3) implies that the chemical potential $\mu(\rho)$ is a nondecreasing function of the density ρ .

⁴¹ In the case of electrically conducting fluid, the present force is *not* an electric one. We have assumed that an electric field only affects the electric carriers, while the present potential couples with the whole fluid.

5.3. Maxwell Relation

A crucial point in our operational definitions of the pressure and the chemical potential is that they automatically imply the Maxwell relation

$$\frac{\partial p(\rho)}{\partial \rho} = \rho \frac{\partial \mu(\rho)}{\partial \rho}, \quad (5.4)$$

which is exactly the same as its equilibrium counterpart (2.17). Here we still fix T , v , and write $p(\rho) = p(T, v; V, N)$ with $\rho = N/V$.

To show the Maxwell relation (5.4), we again consider the situation in Fig. 15, where a varying potential is applied to a single fluid. Suppose that $\Delta u = u_2 - u_1 > 0$ is small. Let us write densities as $\rho_1 = \rho$ and $\rho_2 = \rho - \Delta\rho$. By writing the density $\rho(\mathbf{r})$ and the potential $u(\mathbf{r})$ as a function of the position \mathbf{r} , we can evaluate the total force exerted on the fluid from the potential as

$$\begin{aligned} F_u &= - \int d^3 \mathbf{r} \rho(\mathbf{r}) \text{grad } u(\mathbf{r}) = -\{\rho + O(\Delta\rho)\} \int d^3 \mathbf{r} \text{grad } u(\mathbf{r}) \\ &= -\{\rho + O(\Delta\rho)\} A \Delta u, \end{aligned} \quad (5.5)$$

where A is the cross section area of the container, and we used the fact that $\rho(\mathbf{r}) = \rho + O(\Delta\rho)$ everywhere in the fluid. On the other hand, the forces exerted on the fluid from the upper and lower walls (as pressures) add up to

$$F_p = A\{p(\rho) - p(\rho - \Delta\rho)\}. \quad (5.6)$$

Since the fluid is in a steady state, we must have $F_u + F_p = 0$, which leads to

$$p(\rho) - p(\rho - \Delta\rho) = \rho \Delta u + O((\Delta\rho)^2). \quad (5.7)$$

From (5.3), on the other hand, we have

$$\mu(\rho) - \mu(\rho - \Delta\rho) = \Delta u. \quad (5.8)$$

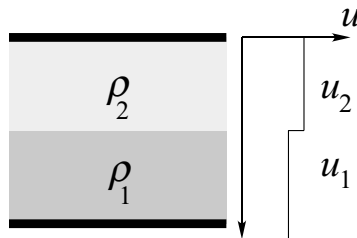


Fig. 15. The method of potential variation which determines the difference in chemical potentials. An external potential which varies only in the vertical direction is applied. The densities of the fluid is ρ_1 and ρ_2 in the lower and the upper regions where the potential takes constant values u_1 and u_2 , respectively. Then the chemical potential difference is determined by $\mu(\rho_1) + u_1 = \mu(\rho_2) + u_2$.

From (5.7) and (5.8), one readily gets the desired Maxwell relation (5.4) by letting $\Delta u \rightarrow 0$.

6. SST FREE ENERGY AND ITS POSSIBLE ROLES

Since we have discussed the operational definitions of the pressure $p(T, v; V, N)$ and the chemical potential $\mu(T, v; V, N)$, we can now move on to the definition of the SST (Helmholtz) free energy $F(T, v; V, N)$. After noting the basic properties of the free energy (Sec. 6.1), we discuss two conjectures about its physical roles, namely, the extension of Einstein's formula for the density fluctuation (Sec. 6.2) and the minimum work principle (Sec. 6.3).

As in Sec. 5, discussions in the present section are fairly general, and apply to any of our examples.

6.1. Definition of Free Energy

Let $(T, v; V, N)$ be a local steady state. Since T and v are intensive, and V and N are extensive, the extensivity of the free energy (to be defined) should read

$$F(T, v; \lambda V, \lambda N) = \lambda F(T, v; V, N), \quad (6.1)$$

for any $\lambda > 0$ (which is small enough to maintain local steadiness). Since this is identical to its equilibrium counterpart (2.4), we expect our SST free energy to satisfy the same Euler equation (2.15) as the equilibrium free energy. We therefore *require*

$$F(T, v; V, N) = -V p(T, v; V, N) + N \mu(T, v; V, N). \quad (6.2)$$

Note that this is consistent with the extensivity (6.1) of free energy and the intensivity (5.1) and (5.2) of the pressure and the chemical potential.

Since we have already determined $p(T, v; V, N)$ and (the V, N dependence of) $\mu(T, v; V, N)$, we can regard the Euler equation (6.2) as our definition of the free energy. This determines the V, N dependence of $F(T, v; V, N)$ completely for each fixed (T, v) . Dependence of $F(T, v; V, N)$ on T and v will be discussed later in Sec. 7.3.

From the Maxwell relation (5.4) (which should better be rewritten in the form of (2.16)), we find that the free energy defined by (6.2) satisfies

$$p(T, v; V, N) = -\frac{\partial F(T, v; V, N)}{\partial V}, \quad (6.3)$$

and

$$\mu(T, v; V, N) = \frac{\partial F(T, v; V, N)}{\partial N}, \quad (6.4)$$

as in the equilibrium thermodynamics (see (2.8) and (2.12)).

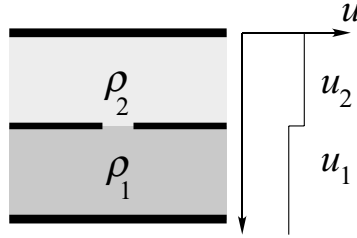


Fig. 16. The setting for discussion the density fluctuation formula (6.9) for nonequilibrium steady states. The situation is almost the same as that of Fig. 15, but the two parts are now separated by a horizontal wall with a small window in it.

We can also show that $F(T, \nu; V, N)$ is jointly convex⁴² in the extensive variables V and N . To see this, fix T and ν and define the specific free energy by

$$f(\rho) = F\left(T, \nu; 1, \frac{N}{V}\right) = \frac{F(T, \nu; V, N)}{V}, \quad (6.5)$$

with $\rho = N/V$. Then the Euler equation (6.2) becomes

$$f(\rho) = -p(\rho) + \rho \mu(\rho). \quad (6.6)$$

From this and the Maxwell relation (5.4), we find $f''(\rho) = \mu'(\rho)$. Since we have $\mu'(\rho) \geq 0$ as argued in Sec. 5.2, $f(\rho)$ is convex in ρ , and hence

$$f\left(\kappa \frac{N_1}{V_1} + (1 - \kappa) \frac{N_2}{V_2}\right) \leq \kappa f\left(\frac{N_1}{V_1}\right) + (1 - \kappa) f\left(\frac{N_2}{V_2}\right), \quad (6.7)$$

for any V_1, V_2, N_1, N_2 , and $0 \leq \kappa \leq 1$. By setting $\kappa = \lambda V_1 / \{\lambda V_1 + (1 - \lambda) V_2\}$ with $0 \leq \lambda \leq 1$, (6.7) becomes

$$\begin{aligned} F(T, \nu; \lambda V_1 + (1 - \lambda) V_2, \lambda N_1 + (1 - \lambda) N_2) &\leq \lambda F(T, \nu; V_1, N_1) \\ &+ (1 - \lambda) F(T, \nu; V_2, N_2), \end{aligned} \quad (6.8)$$

which shows the desired convexity.

6.2. Density Fluctuation

Although we still do not know T, ν dependence of the free energy $F(T, \nu; V, N)$, its dependence on V and N may give interesting physical information. In the present and the next subsections, we discuss two of such conjectures.

Consider the situation in Fig. 16, where the potential which is equal to u_1 in the lower half and equal to u_2 in the upper half is applied. This is almost the

⁴² See footnote 13 in Sec. 2.1.2 for the definition. The following discussion is quite standard.

same as the situation in Fig. 15, but we separate the two parts by a horizontal wall with a small (but much larger from the molecular scale) window in it. The wall is prepared so that the two parts maintain the same “degree of nonequilibrium.” Since the two parts will reach mechanical and thermodynamic balance via the window, the densities ρ_1 and ρ_2 in the steady state is the same as that attained in the situation of Fig. 15.

In the average, the amounts of fluid in the two parts are equal to $\rho_1 V$ and $\rho_2 V$, respectively, where V is the volume of each part. As long as the volume is finite, however, there exists a fluctuation in the amounts of fluid or in the densities. We conjecture that *this density fluctuation can be described by the SST free energy*, just as in the equilibrium case (2.6). (See also (2.22).) To our knowledge, such a fluctuation relation in steady states was first proposed by Hayashi and Sasa⁽⁴⁷⁾.

To be precise, denote the amounts of substance in the lower and the upper parts as N_1 and N_2 , respectively. Since the fluid can move through the porous wall, N_1 and N_2 may vary while $N_1 + N_2$ is exactly conserved. We denote by $\tilde{p}(N_1, N_2)$ be the probability density for the partition (N_1, N_2) of the amounts of fluid. Then, for each steady state with fixed T , v , u_1 , and u_2 , it is expected that the Einstein’s formula

$$\tilde{p}(N_1, N_2) \simeq \text{const.} \exp[-\beta\{F(T, v; V, N_1) + F(T, v; V, N_2) + u_1 N_1 + u_2 N_2\}], \quad (6.9)$$

is valid, where $\beta = 1/(k_B T)$ is the inverse temperature.

We shall later show that the fluctuation formula (6.9) holds exactly in the sheared fluid with weak contact (Appendix A.3), and the driven lattice gas (Appendix B.4).

It is quite important to note that the conjectured relation (6.9) can be checked by experiments which are independent of those necessary to determine the free energy $F(T, v; V, N)$. Therefore we are proposing a highly nontrivial statement for general (not necessarily weak) nonequilibrium systems that can be verified (or falsified) purely by experiments. See Sec. 8.2.1 for further discussions.

Remark 1: When the density fluctuation is governed by the Einstein’s formula (6.9), it is likely that linear response relations for transport or relaxation phenomena in the *vertical* direction are also valid. For example, if one starts from the steady state with $u_1 = u_2 = 0$ and suddenly applies at time $t = 0$ a weak potential difference $\Delta u = u_2 - u_1$, we expect the fluctuation response relation

$$\langle \hat{N}_1(t) \rangle_{\Delta u} = \langle \hat{N}_1 \rangle_0 + \Delta u \beta \langle \hat{N}_1 \{ \hat{N}_1(t) - \hat{N}_1(0) \} \rangle_0 + O((\Delta u)^2), \quad (6.10)$$

for $t \geq 0$ to be valid. Here $\langle \cdots \rangle_0$ is the expectation in the steady state with $u_1 = u_2 = 0$. See Secs. A.4 and B.6 for more details in concrete examples. To our knowledge, such linear response relations in a highly nonequilibrium steady state was first discussed in Ref. 84.

Remark 2: One might naively expect the fluctuation relation (6.9) to hold in the situation of Fig. 15, where the two parts are separated by a *fictitious* horizontal plane. Although the corresponding relation in equilibrium holds either when the wall is real or fictitious, the situation may not be that simple in nonequilibrium steady states. In nonequilibrium steady states, one generally finds spatial long range correlations, which lead to anomalous density fluctuations.⁽²⁰⁾ (See Sec. 8.3.2.) It is likely that a simple Einstein type relation for fluctuation does not hold because of this anomaly. The contact via a small window considered above is expected to diminish the long range correlation between the two subsystems, while maintaining macroscopic balance of the two systems. This is clearly seen in our treatment of the driven lattice gas in Appendix B.3. See also Appendix B.3.4 for still “safer” design of the contact.

6.3. Minimum Work Principle

We also conjecture that there exists a steady state version of the minimum work principle (see Sec. 2.1.2) and that the SST free energy plays a central role in it.

Let us discuss only the simplest version in the present section. Later in Appendix B.5 we shall discuss more about the minimum work principle in the contexts of driven lattice gas.

We conjecture that a straightforward generalization of the inequality (2.5) in equilibrium holds in a local steady state. However there is a sever restriction on mechanical operations performed to the system. To be consistent with our basic framework to change the geometry of the system only in the vertical direction, we allow the external agent to change the volume of the system only by moving the upper (or the lower) wall vertically. We require that the intensive variables T and ν are kept constant during the operation. Then the conjectured minimum work principle for local steady states is

$$W \geq F(T, \nu; V', N) - F(T, \nu; V, N), \quad (6.11)$$

where V and V' are the initial and the final volumes, respectively, and W is the mechanical work that the outside agent has done to the system. It is crucial here that W is the ordinary mechanical work, not an exotic (and often ill-defined) quantity like “nonequilibrium work.”⁴³ The outside agent need not care whether the system is in an equilibrium state or in a steady state.

⁴³ In the framework of SST proposed by Oono and Paniconi⁽²⁾, the conjectured minimum work principle is expressed in terms of “excess work” which is obtained by subtracting a “house-keeping heat” from the total mechanical work. Such a decomposition of the work with a generalized second law was demonstrated in a Langevin model.⁽⁸⁵⁾ Quite recently, an identity leading to this generalized second law was tested experimentally Ref. 86.”

In the limit where the operation is indefinitely slow, the relation (6.3) for the pressure implies that the minimum work principle (6.11) is satisfied as an equality. (This is indeed almost the definition of the pressure.) Then the conjectured inequality (6.11) looks plausible since we usually have to do extra work when an operation is not slow enough for the fluid to follow.

We stress that the restriction on allowed operations is essential. Since some of the nonequilibrium steady states have a macroscopic flow, the agent may make use of it to reduce her work (or even to get a positive amount of energy from, say, a waterwheel) if arbitrary operations are allowed. This is in a stark contrast with the minimum work principle in the equilibrium thermodynamics, where the agent can perform any mechanical operations allowed by physics laws.

To summarize, our message is that *the minimum work principle may be extended to general nonequilibrium steady states provided that one carefully restricts allowed operations*. We stress that this too is a highly nontrivial conjecture that can be checked purely by experiments.

7. STEADY STATE THERMODYNAMICS (SST) IN A COMPLETE FORM

In the present section, we discuss an operational method to determine the dependence of the chemical potential on T and v . The basic idea depends on a new postulate that there are walls (that we call μ -walls) which realize a natural contact between an equilibrium state and a steady state (Secs. 7.1 and 7.2). This determines the free energy $F(T, v; V, N)$ (Sec. 7.3), and completes our construction of steady state thermodynamics (SST).

The complete SST leads us to predictions of two new phenomena, namely, the flux-induced osmosis (FIO) (Secs. 7.4 and 7.5), and a shift of coexistence temperature (Sec. 7.6). We show that both the phenomena are described by the new nonequilibrium extensive quantity $\Psi(T, v; V, N)$ that we shall introduce. These two are intrinsically nonequilibrium phenomena that can never be described within the equilibrium or the local equilibrium treatments.

7.1. Contact of a Steady State and an Equilibrium State

As in Secs. 5 and 6, we treat a general local steady state parameterized as $(T, v; V, N)$.

We shall now think about bringing a local steady state $(T, v; V, N)$ in contact with an equilibrium state $(T, 0; V', N')$, allowing the two states to slowly exchange the fluid. To be consistent with the general scheme of SST, we put the two states together in the vertical direction, separating them with a horizontal wall.

The separating wall should probably be made of a porous material which has many narrow complicated paths through which the fluid can pass slowly.

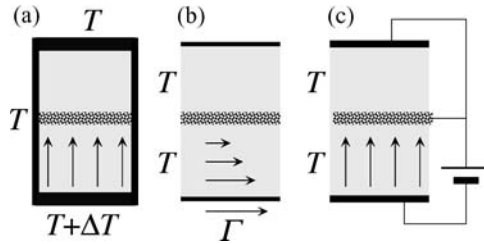


Fig. 17. Combination of a nonequilibrium steady state (lower part) and an equilibrium state (upper part) in (a) heat conducting fluid, (b) sheared fluid, and (c) electrical conduction in a fluid. The separating walls are made of a porous material, and fluid can pass to the other sides through narrow complicated paths. This setting will be the basis for our determination of the chemical potential and the free energy.

In the case of a heat conducting fluid (Sec. 3.1.1), we suppose that the porous wall has very high heat conductivity, and is in touch with a heat bath which has the same temperature T as the upper most wall. See Fig. 17(a). The lower most wall is kept at a different temperature $T + \Delta T$. In this manner, we can realize a heat conducting (local) steady state in the lower half of the system, and an equilibrium state with temperature T in the upper half of the system.

In the case of a sheared fluid (Sec. 3.1.2), we suppose that porous wall has “sticky” surfaces and is at rest. See Fig. 17(b). The upper most wall is also at rest, while the lower most wall moves with the speed Γ . In this manner, we realize a (local) steady state with a constant shear in the lower half, and an equilibrium state in the upper half. We of course assume that the whole system is in an efficient contact with a heat bath at temperature T .

As for electrical conduction in a fluid (Sec. 3.1.3), we have to be careful. When we employ the $(T, \phi; V, N)$ formalism of SST (see Fig. 13(b)), it is impossible to put an equilibrium state on top of a steady state. This is because a steady state in this setting has a uniform electric field in the horizontal direction in it, while an equilibrium state has no electric field. Such a configuration is inhibited by the law of electrostatics, i.e., $\text{rot } \mathbf{E} = 0$. We therefore exclude the $(T, \phi; V, N)$ formalism from our considerations in the present section.

As for the $(T, I; V, N)$ formalism of SST for electrical conduction in a fluid (see Fig. 13(a)), the contact causes no apparent problems. We suppose that the porous wall is electrically conducting, and let the porous wall and the upper most wall have the same electric potential. See Fig. 17(c). By letting the the lower most wall have a different potential, we will get a steady state with a constant electric current in the lower half, and an equilibrium state in the upper half. Again the whole system is assumed to be in touch with a heat bath at temperature T .

7.2. Complete Determination of the Chemical Potential

Our new (and fundamental) postulate is that, if a steady state $(T, \nu; V, N)$ and an equilibrium state $(T, 0; V', N')$ are in contact with each other as in Sec. 7.1, we have the equality

$$\mu(T, \nu; V, N) = \mu(T, 0; V', N'). \quad (7.1)$$

In equilibrium thermodynamics, two systems which exchange substance and are in balance with each other always have equal chemical potentials. Our postulate (7.1) is a straight generalization of this principle.

Since $\mu(T, 0; V', N')$ in the right-hand side is the chemical potential of an equilibrium state, it is fully determined within the equilibrium thermodynamics. Therefore by preparing the contact between various steady states and equilibrium states, one can fully determine the SST chemical potential $\mu(T, \nu; V, N)$ from the proposed equality (7.1).

It must be noted, however, that (7.1) is not a mere definition. In Sec. 5.2, we characterized the chemical potential $\mu(T, \nu; V, N)$ using the method of potential variation, and determined the V, N dependence of $\mu(T, \nu; V, N)$ for each fixed T and ν . The equality (7.1) must reproduce the same V, N dependence.

Therefore what is essential in the postulate (7.1) is the assumption that *there exists a wall which (through (7.1)) gives $\mu(T, \nu; V, N)$ consistent with the potential variation method*. Let us call a wall with this property a μ -wall. The existence of a perfect μ -wall is indeed far from obvious (although it can be established for the driven lattice gas as we see in Sec. B.7). In fact we will see in Sec. 7.5 that there are walls which are *not* μ -walls. The validity of our postulate should ultimately be verified through series of careful experiments.

We assume that the chemical potential thus defined satisfies the symmetry

$$\mu(T, \nu; V, N) = \mu(T, -\nu; V, N). \quad (7.2)$$

For a sheared fluid this is obvious from the original symmetry (i.e., Galilei invariance) of the system. For heat conduction and electrical conduction, we are assuming that the direction of the current does not affect the contact with equilibrium state. This is not entirely obvious, but seems plausible. Similarly we assume for the pressure that

$$p(T, \nu; V, N) = p(T, -\nu; V, N). \quad (7.3)$$

7.3. Complete Determination of the Free Energy

Since we have completely determined the chemical potential $\mu(T, \nu; V, N)$, and the pressure $p(T, \nu; V, N)$, we use the Euler equation (6.2) to fully determine the free energy $F(T, \nu; V, N)$.

The free energy $F(T, \nu; V, N)$ thus defined satisfies the extensivity (6.1), is jointly convex in V and N (as we saw in Sec. 6.1), and has the symmetry

$$F(T, \nu; V, N) = F(T, -\nu; V, N), \quad (7.4)$$

because of (7.2) and (7.3). Trusting in robustness of the mathematical structure of thermodynamics, we further assume that the free energy $F(T, \nu; V, N)$ is concave in the two intensive variables T and ν . Although it is a general requirement in thermodynamics that the free energy is concave in an intensive variable, we still do not know what this assumption really means in the context of nonequilibrium steady states.⁴⁴

Assuming the differentiability of $F(T, \nu; V, N)$, we can define (following equilibrium thermodynamics) the SST entropy

$$S(T, \nu; V, N) = -\frac{\partial F(T, \nu; V, N)}{\partial T}, \quad (7.5)$$

and a new nonequilibrium extensive quantity

$$\Psi(T, \nu; V, N) = -\frac{\partial F(T, \nu; V, N)}{\partial \nu}. \quad (7.6)$$

Since the symmetry (7.4) implies $\Psi(T, \nu; V, N) = -\Psi(T, -\nu; V, N)$, we find that $\Psi(T, 0; V, N) = 0$ provided that $\Psi(T, \nu; V, N)$ is continuous in ν . Moreover the assumed concavity of $F(T, \nu; V, N)$ implies

$$\frac{\partial \Psi(T, \nu; V, N)}{\partial \nu} \geq 0, \quad (7.7)$$

and hence we have

$$\Psi(T, \nu; V, N) \begin{cases} \geq 0 & \text{if } \nu \geq 0; \\ = 0 & \text{if } \nu = 0; \\ \leq 0 & \text{if } \nu \leq 0. \end{cases} \quad (7.8)$$

Since the inequalities (7.8) suggest that $\Psi(T, \nu; V, N)$ is a kind of measure of the “degree of nonequilibrium,” we call $\Psi(T, \nu; V, N)$ the *nonequilibrium order parameter*.⁴⁵

⁴⁴ In equilibrium thermodynamics, the concavity is directly related to the convexity and the variational principle for the conjugate extensive variable. To find out whether we have similar structure in SST is one of the important remaining issues. There is a possibility that we should use a monotone function $\psi(\nu)$ of ν as the “correct” intensive nonequilibrium variable to have a meaningful conjugate extensive variable.

⁴⁵ As a simple minded analogy, imagine that ν is the external magnetic field of a magnetic system. Then Ψ becomes the magnetization.

7.4. Flux Induced Osmosis (FIO)

We continue to study the situation in Fig. 17, where a local steady state $(T, \nu; V, N)$ and an equilibrium state $(T, 0; V', N')$ are in contact with each other. Thus the equality (7.1) between the chemical potentials hold.

Let us think about changing the nonequilibrium control parameter ν slightly while keeping the temperature T , the volume V , and the equilibrium chemical potential $\mu_{\text{eq}} = \mu(T, 0; V', N')$ constant. The last condition is met, for example, by making V' and N' much larger than V and N , respectively. Since the chemical potential $\mu(T, \nu; V, N)$ must be also constant because of (7.1), the amount of substance N in the steady state inevitably varies according to ν . In what follows we write $N(\nu)$ instead of N to remind this fact.

By dividing the Euler equation (6.2) by N and using the extensivity (6.1) of F and the intensivity (5.1), (5.2) of p, μ , we get

$$F(T, \nu; \nu, 1) = -\nu p(T, \nu; \nu, 1) + \mu(T, \nu; \nu, 1), \quad (7.9)$$

where $\nu = V/N(\nu)$ is the specific volume. When the nonequilibrium variable ν is varied, T and $\mu(T, \nu; \nu, 1)$ do not change while ν may change. Thus by differentiating (7.9) with respect to ν , we get

$$-\Psi(T, \nu; \nu, 1) - \frac{\partial \nu}{\partial \nu} p(T, \nu; \nu, 1) = -\frac{\partial \nu}{\partial \nu} p(T, \nu; \nu, 1) - \nu \frac{\partial p(T, \nu; \nu, 1)}{\partial \nu}, \quad (7.10)$$

where we used (7.6) and (6.3). This implies

$$\frac{\partial p(T, \nu; V, N(\nu))}{\partial \nu} = \frac{\Psi(T, \nu; V, N(\nu))}{V}. \quad (7.11)$$

Since the pressure $p(T, \nu; V, N(\nu))$ is equal to the equilibrium pressure $p_{\text{ea}} = p(T, 0; V', N')$ when $\nu = 0$, and the sign of the right-hand side of (7.11) is given by (7.8), we find that

$$p(T, \nu; V, N(\nu)) \geq p_{\text{eq}}, \quad (7.12)$$

in general. For $\nu \neq 0$, the inequality is expected to become strict except in trivial systems where $\Psi(T, \nu; V, N)$ is vanishing.

We thus conclude that *there inevitably appears a difference in the pressures of a nonequilibrium steady state and an equilibrium state* which are in contact with each other and exchanging the fluid. The assumed concavity of the free energy in the nonequilibrium intensive parameter ν implies that the pressure of the steady state is always higher. We call this pressure difference the *flux-induced osmosis* (FIO).

We stress that the FIO is an intrinsically nonequilibrium phenomenon, which can never be predicted within the standard local equilibrium approach (see Sec. 1.3.1). To confirm the existence of a FIO through careful experiments seems

to be a challenging task, which will shed completely new light on the physics of nonequilibrium systems. We note, however, that an actual design of experiment may be nontrivial. See Sec. 8.2.2.

The prediction of FIO in a heat conducting system may be rather surprising since we assert that a transfer of heat leads to a mechanical force acting on the porous wall. Let us note, however, that the appearance of mechanical force may not be too radical at least for dilute gases. In a dilute gas with a nonuniform temperature profile, it is known from the analysis of the Boltzmann equation that the pressure tensor becomes anisotropic.⁽³³⁾ It is then possible that a nonequilibrium steady state and an equilibrium state balance with each other to have different vertical pressures. In fact Kim and Hayakawa,⁽³⁵⁾ in their careful reinvestigation of the Chapman-Enskog expansion, examined a naive contact between a nonequilibrium steady state and an equilibrium state, and found that the pressure of the steady state is indeed larger than that of the equilibrium state.⁴⁶ A recent calculation based on Enskog's equation leads to a different conclusion.⁽⁸⁷⁾

7.5. μ -Wall Revisited

Since the existence of a μ -wall inevitably leads to the pressure difference between the steady state and the equilibrium state, we find that a μ -wall must be able to support a pressure difference. But clearly there exists a wall (which should be called a p -wall) which ensures that the pressures on its two sides are identical. For example, a "wall" made of a network of thin wires may be able to separate a steady state and an equilibrium state, but cannot support a pressure difference. In this case, we must conclude that there is a finite difference in the chemical potentials of the steady state and the equilibrium state, while the pressures are the same. This is in a sharp contrast with the situation in equilibrium thermodynamics, where any contact which allows the exchange of fluid keeps the chemical potential on both sides equal.

We suspect that a perfect μ -wall and a perfect p -wall represent two different idealized limits of experimentally realizable walls. A general wall separating a steady state and an equilibrium state is expected to lie between these two limits. For a non-ideal wall, we still expect to observe a FIO with the same sign, but with a reduced magnitude.

Let us derive a useful relation which enables one to check if an ideal μ -wall contact is realized or not. Suppose that a steady state $(T, \nu; V, N)$ and an equilibrium state $(T, 0; V', N')$ are separated by a perfect μ -wall and are in balance with each other. We fix T and ν , and slightly change the density by varying V or V' . Since both the steady state pressure $p_{ss} = p(T, \nu; V, N)$ and

⁴⁶ Although they found a FIO with the correct sign, their contact is not a perfect μ -wall since the equality (7.13) is violated. We still do not know how one should realize a perfect μ -wall in dilute gases.

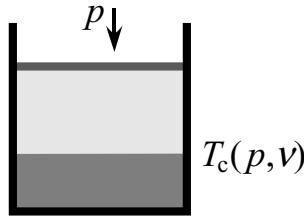


Fig. 18. Two phases (say, liquid and vapor) separated by a horizontal plane coexist within a nonequilibrium steady state. We show that in general the coexistence temperature $T_c(p, v)$ shifts from its equilibrium value $T_c(p, 0)$.

the equilibrium pressure $p_{eq} = p(T, 0; V', N')$ satisfy the same Maxwell relation (2.16) and (5.4), the changes of the pressures satisfy $\Delta p_{eq} = \rho_{eq} \Delta \mu_{eq}$ and $\Delta p_{ss} = \rho_{ss} \Delta \mu_{ss}$, where $\Delta \mu_{eq}$ and $\Delta \mu_{ss}$ are the changes in the chemical potentials. But (7.1) implies $\Delta \mu_{eq} = \Delta \mu_{ss}$, and we get

$$\frac{\Delta p_{eq}}{\Delta p_{ss}} = \frac{\rho_{eq}}{\rho_{ss}}. \tag{7.13}$$

The equality (7.13) may be checked experimentally to see if an ideal μ -wall is realized.

7.6. Shift of Coexistence Temperature

Again we consider a single local steady state. Suppose that there coexist two different phases, say, liquid and vapor, within the local steady state. We assume that the two phases are separated by a horizontal plane as in Fig. 18. By using standard techniques in thermodynamics, we derive a nonequilibrium relation corresponding to the Clausius-Clapeyron relation.

By (fictitiously) splitting the system into two along the phase separation plane, we get two local steady states in the low and the high temperature phases, respectively. We denote the local steady states in the low and the high temperature phases as $(T, v; V_-, N_-)$ and $(T, v; V_+, N_+)$, respectively.

By dividing the Euler equation (6.2) by N and using the extensivity (6.1) of F and the intensivity (5.1), (5.2) of p, μ , we get for each phase

$$F(T, v; v_{\pm}, 1) = -v_{\pm} p(T, v; v_{\pm}, 1) + \mu(T, v; v_{\pm}, 1), \tag{7.14}$$

where $v_{\pm} = V_{\pm}/N_{\pm}$ are the specific volumes. It is convenient to fix the pressure $p = p(T, v; v_-, 1) = p(T, v; v_+, 1)$ constant. We denote by $T_c(p, v)$ the coexistence temperature at fixed p and v . Since the two phases coexist, we have⁴⁷

⁴⁷One may regard this balance condition as a special case of (5.3).

$\mu(T, v; v_-, 1) = \mu(T, v; v_+, 1)$, which, with (7.14), implies

$$F(T_c(p, v), v; v_-, 1) + v_- p = F(T_c(p, v), v; v_+, 1) + v_+ p. \quad (7.15)$$

We fix p and differentiate (7.15) with respect to v . Noting that v_{\pm} may depend on v to keep the pressure constant, we get

$$\begin{aligned} & -\frac{\partial T_c(p, v)}{\partial v} S(T_c(p, v), v; v_-, 1) - \Psi(T_c(p, v), v; v_-, 1) \\ & = -\frac{\partial T_c(p, v)}{\partial v} S(T_c(p, v), v; v_+, 1) - \Psi(T_c(p, v), v; v_+, 1), \end{aligned} \quad (7.16)$$

where we used the definitions (7.5) and (7.6) of S and Ψ , respectively. We therefore find the following nonequilibrium relation analogous to the Clausius-Clapeyron relation

$$\frac{\partial T_c(p, v)}{\partial v} = -\frac{\psi_+ - \psi_-}{s_+ - s_-}, \quad (7.17)$$

where

$$\psi_{\pm} = \frac{\Psi(T_c(p, v), v; V_{\pm}, N_{\pm})}{V_{\pm}}, \quad (7.18)$$

and

$$s_{\pm} = \frac{S(T_c(p, v), v; V_{\pm}, N_{\pm})}{V_{\pm}} \quad (7.19)$$

are the specific nonequilibrium order parameter and the specific entropy of the two phases.

It is crucial to note that the nonequilibrium order parameter ψ_{\pm} can be determined by experiments using the FIO of Sec. 7.4. Since the entropy s_{\pm} may be approximated by their equilibrium values for small enough v , the right-hand side of (7.17) can be evaluated from experiments which do *not* involve a phase coexistence. This enables one to check (at least in principle) for the *quantitative validity* of the theory of SST in a purely experimental manner.

The concavity of the free energy implies that in general the entropy $S(T, p, v; N)$ is nondecreasing⁴⁸ in T . Thus we always have $s_+ \geq s_-$, and expect

$$s_+ - s_- > 0, \quad (7.20)$$

in general. Therefore the sign of the right-hand side of the Clausius-Clapeyron type relation (7.17) is determined by the sign of $\psi_+ - \psi_-$.

⁴⁸To show this one Legendre transforms $F(T, v; V, N)$ to $G(T, p, v; N)$ and use the relation $S = -\partial G/\partial T$ as in equilibrium thermodynamics.

Consider a sheared fluid and suppose that the low temperature phase is a solid.⁴⁹ Since the solid phase is hardly affected by the shear, it is likely that ψ_- is negligible. Then the relation (7.17) becomes

$$\frac{\partial T_c(p, \tau)}{\partial \tau} = -\frac{\psi_+}{s_+ - s_-}. \quad (7.21)$$

The sign of the right-hand side of (7.21) is precisely known by (7.8) and (7.20). We find that

$$T_c(p, \tau) < T_c(p, 0), \quad (7.22)$$

in general. Shear always induces melting of a solid. This prediction is consistent with the recent numerical experiments⁽⁸⁸⁾ (where it was argued that the inequality (7.22) rules out (!) the possibility of a nonequilibrium thermodynamics).

It is especially interesting to investigate experimentally the possible shift of coexistence temperature in a system with heat flow. The right-hand side of (7.17) may be positive or negative depending on systems. If $T_c(p, J) > T_c(p, 0)$, one will find a remarkable phenomenon of “heat flux induced condensation,” i.e., one observes condensation of a low temperature phase near one of the walls which have slightly *higher* temperature than the normal transition temperature while the other wall has much higher temperature!

8. DISCUSSIONS

8.1. Summary and Perspective

In the present work, we have step by step developed a full fledged thermodynamics that is expected to apply to a wide class of nonequilibrium steady states. We have tried hard to be as clear as possible in explaining our basic assumptions and reasoning behind the construction. We believe that our consideration about possible extensions of thermodynamics to nonequilibrium steady states is much more careful and rigorous than any other existing attempts.

We have developed our theory in the level of purely macroscopic phenomenology, and clarified what conclusions we get from only phenomenological considerations. All thermodynamic quantities are defined through experimentally realizable operations. We also made some nontrivial predictions that can be tested empirically. We shall discuss about possible experimental tests in Sec. 8.2.

The reader may have noticed that there are, roughly speaking, three stages in our theory of SST. The first stage, developed in Secs. 3 and 4, deals with very basic framework of SST. We have examined basic symmetries of nonequilibrium steady states and fundamental structures of thermodynamics, and made a rather

⁴⁹To consider a solid phase goes beyond our framework to treat only fluids. But let us be optimistic.

strong restriction on possible theories. The second stage, developed in Secs. 5 and 6, deals with thermodynamics with fixed T and ν . We have discussed important physics (the minimum work principle and the density fluctuation formula) that can be read off from the V, N dependence of the SST free energy. The third stage, developed in Sec. 7, deals with SST in a complete form. We predicted the FIO and the shift of coexistence temperature.

We believe that the logic in the first and the second stage is reasonably firm and reliable. Although a sound logic does not necessarily mean the validity of the theory, we are rather confident that our theory is realized in some nonequilibrium systems in nature. The theory in the third stage is definitely most interesting, but its logic is not as firm as the previous ones. First the notion of μ -wall is not yet perfectly clear from an operational point of view, and must be further examined. Secondly, our assumption about the concavity of the SST free energy depends solely on the analogy with the conventional thermodynamics and has no operational foundation. We nevertheless wish to encourage experimental works for testing our predictions related to μ -wall contacts and clarifying the nature of contacts between equilibrium states and nonequilibrium steady states. Either verification or falsification of our predictions will provide hints for future development in nonequilibrium physics.

A crucial point about the potential significance of SST is whether it becomes a useful guide in the (future) construction of statistical mechanics for steady nonequilibrium states. The fact that we have arrived at an essentially unique theory is rather encouraging. We hope that, by trying to construct a statistical theory that is consistent with the (unique) nonequilibrium thermodynamics, we are naturally led to a meaningful and correct statistical mechanics for steady nonequilibrium states. We shall discuss related issues in the Appendix , where we look at SST from a microscopic point of view.

8.2. Possibility of Experimental Tests

Let us briefly discuss possible experimental verification of our predictions. Our aim here is not to go into details of concrete experimental setups but to make clear some essential points in our theory which need to be tested empirically.

8.2.1. Chemical Potential and Fluctuation

Probably the most promising experiments of SST are those designed to verify the formula for density fluctuation in nonequilibrium steady states (and the corresponding fluctuation-response relations) discussed in Sec. 6.2.

For this, one should prepare a system which is separated into two by a wall (which realizes a weak contact of the two subsystems), and in which an external potential can be varied. One then realizes a nonequilibrium steady state in the

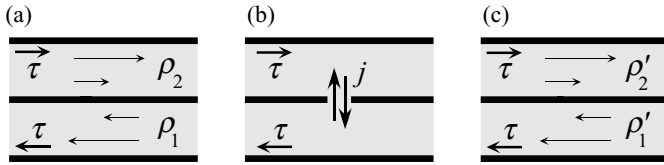


Fig. 19. The scheme of weak contact for a sheared fluid. The upper and the lower parts are separated by a horizontal wall which has a small window in it. (a) Both the lower and the upper parts are in their steady states. (b) The window opens for a finite interval of time, allowing some fluid to move. We denote by j the total amount of fluid that have moved from the lower to the upper part. (c) The window closes, and again both parts settle into their steady states with new densities. We repeat this process many times and discuss the balance between the two parts, density fluctuation, and linear response.

system. See, for example, Figs. 16 and 19. One should also be able to measure the amounts of substance in the two subsystems accurately.⁵⁰

In the first stage of experiments, one fixes T , ν , and measures the averaged amounts of substance for various (fixed) values of the potential difference $u_2 - u_1$. Then by using these data and the definition (5.3) of the chemical potential, one can experimentally determine $\mu(\rho)$ (up to an arbitrary additive constant). Of course nothing has been verified at this stage.

In the second stage of experiments (which may of course be carried out at the same time as the first stage), one measures the fluctuation of the amounts of substance N_1, N_2 in the two subsystems, again for fixed u_1 and u_2 . Then our conjecture is that the probability to observe a partition into N_1 and N_2 behaves as

$$\tilde{p}(N_1, N_2) \propto \exp[-\beta\{F(V_1, N_1) + u_1 N_1 + F(V_2, N_2) + u_2 N_2\}], \quad (8.1)$$

where we dropped T and ν . We have extended (6.9) to treat the case where the two regions have volumes V_1 and V_2 . This enables us to get as much information as possible from this setting.

Now if the fluctuation is small (which seems to be always the case in actual experiments for large systems), one may expand the above formula (8.1) to get

$$\tilde{p}(\Delta N) \propto \exp\left[-\frac{\beta}{2} \left\{ \frac{\partial}{\partial N_1} \mu\left(\frac{N_1^*}{V_1}\right) + \frac{\partial}{\partial N_2} \mu\left(\frac{N_2^*}{V_2}\right) \right\} (\Delta N)^2\right], \quad (8.2)$$

where N_1^* and N_2^* are most likely values of the amounts of substance determined by $\mu(N_1^*/V_1) + u_1 = \mu(N_2^*/V_2) + u_2$, and $\Delta N = N_1^* - N_1 = N_2 - N_2^*$ is the deviation. Thus the variance of the deviation ΔN is given by

$$\langle(\Delta N)^2\rangle = \frac{1}{\beta} \left\{ \frac{\mu'(\rho_1^*)}{V_1} + \frac{\mu'(\rho_2^*)}{V_2} \right\}^{-1}, \quad (8.3)$$

⁵⁰ A hopeful candidate is a system of charged plastic beads floating in water.

where $\rho_i^* = N_i^*/V_i$.

It must be noted that only $\mu'(\rho)$ (not $\mu(\rho)$ itself) appears in the formula (8.3) of the variance. Since one has determined $\mu'(\rho)$ unambiguously in the first stage, one can now check for the quantitative validity of (8.3). Note also that one can increase the reliability of the conclusion by carrying out experiments with various values of $u_2 - u_1$, and V_1, V_2 .

As we shall discuss in Sec. 8.3.1, there is a possibility that the inverse temperature β in (8.3) should be replaced with an “effective inverse temperature.” Even if this is the case, a series of experiments with varying $u_2 - u_1$, V_1 , and V_2 is enough to check for the quantitative validity of the conjectured formula (8.3).

Moreover, one can determine the effective inverse temperature from a completely independent set of measurements. One can measure relaxation process which takes place after suddenly changing the potential difference, and compare it with static temporal correlations through the fluctuation-response relations like (6.10) or those described in Secs. A.4 and B.6. Since the parameter β appearing in fluctuation-response relations should be the same as those in the density fluctuation formula, this makes our proposal of experiments completely nontrivial. See also Sec. A.5 for the similar discussion.

The minimum work principle (6.11) may be also checked empirically, but we still do not know what can be conclusive experiments.

8.2.2. Flux Induced Osmosis

There is no doubt that the most exciting experimental verification of our SST is to directly observe flux-induced osmosis (FIO), especially in a heat conducting state, and directly measure the nonequilibrium order parameter Ψ . Unfortunately this project seems still not easy to carry out for several reasons. One essential difficulty is that we still do not know how one can realize a perfect μ -wall, which is necessary for a measurement of Ψ . We imagine that a search for sufficiently good μ -walls should be done through a series of careful experiments using various different walls.

Therefore the first step will be to confirm the existence of FIO in a system with not necessarily perfect μ -wall. This alone, we believe, can be an essential step toward a better understanding of truly nonequilibrium systems. But even this may not be easy since we have almost no a priori estimate for the magnitude of the pressure difference. The lack of quantitative estimates is characteristic to any thermodynamic arguments. Thermodynamics provides us with universal and exact relations, but not with numerical estimates.

For dilute gases, however, we can make some rough estimates based on kinetic theory. Consider a heat conducting state of a dilute gas. We want to examine the dimensionless quantity $\theta = (p_{ss} - p_{eq})/p_{eq}$ which characterizes the magnitude of the FIO. Let j be the heat flux per unit area. Since θ should be an even function of

j , it is expected that θ is proportional to j^2 when j is small. Then the dimensional analysis shows that the only dimensionless combination (that includes j^2) of basic quantities is

$$\theta \sim \frac{mj^2}{p^2kT}, \quad (8.4)$$

where m is the mass of the gas molecule. Of course p (which may be either p_{eq} or p_{ss}) is the pressure and T is the temperature. This indeed is roughly equal to the magnitude of the anisotropy of the pressure tensor obtained from the Chapman-Enskog expansion.⁽³³⁾ The FIO obtained in the dilute gas calculation by Kim and Hayakawa⁽³⁵⁾ also has the same order of magnitude.

To first confirm that FIO is negligibly small in the ordinary environment, let us examine the Ar gas at $T = 273$ K and $p = 1$ atm. The heat flux is given by $j = \kappa(\nabla T)$ with the thermal conductivity $\kappa \simeq 2.1 \times 10^{-2} \text{ J(s m K)}^{-1}$. As for the temperature gradient, let us set for the moment $\nabla T = 10^4 \text{ K/m}$ (i.e., 100 K difference within 1 cm, which is easily realizable in the kitchen). By using $m \simeq 6.0 \times 10^{-26} \text{ kg}$, we get $\theta \sim 5 \times 10^{-11}$, which is miserably small as we anticipated.

To get more general estimate and see what we can do, we further use the results from the gas kinetic theory to write

$$j \sim \sqrt{\frac{kT}{m}} \frac{k(\nabla T)}{d^2}, \quad (8.5)$$

where d is the hard core diameter of the gas molecule. Then we get

$$\theta \sim \frac{k^2(\nabla T)^2}{d^4 p^2}, \quad (8.6)$$

which is independent of T . The formula means that we must have low pressure as well as large temperature gradient in order to observe a large nonequilibrium effect. Let us set $p = 10$ Pa, for example, where the mean free path at room temperature is still not too large. Let us require $\theta \sim 10^{-2}$ since a difference of 0.1 Pa may be detected by a diaphragm. Then since $d \sim 10^{-10} \text{ m}$, we need to have $\nabla T \sim 10^3 \text{ K/m}$, which may not be too unrealistic. Perhaps a major challenge in the realization of this experiment is to control convection and other non-thermodynamic effects. It was clearly pointed out in Ref. 89 that, in a naive setting of FIO, the pressure difference due to the boundary effect (namely, the temperature gap) is proportional to the heat flux j , and hence overwhelms the effect predicted by SST. Therefore one should devise a special setting in which the temperature gap is eliminated to reveal the effect proportional to j^2 (See also Sec. 8.3.3).

As for systems other than dilute gases, we have no estimates for FIO. We may simply hope that the nonequilibrium effects become large in some complex fluids.

The conjectured shift of coexistence temperature is also an interesting topic of experiments. In this case, however, we have no a priori estimate at all. It is quite

interesting to know if experiments like the one described in Refs. 90 and 91 have any relations with our predictions.

8.3. Frequently Asked Questions

During these four years that we have spent developing the present theory, we were repeatedly asked some important questions in conferences, seminars, personal discussions, and referee reports. We shall summarize below our answers to some of these “frequently asked questions.”

Probably the most frequently asked question was about the possible relation of SST to some of the existing attempts in nonequilibrium physics. This is why we prepared Sec. 1.3, where we listed some of the major advances in nonequilibrium physics and discussed their relevance (or irrelevance) to SST. We then concluded that there have been essentially nothing really similar to SST, concerning either basic philosophy or concrete theories.

8.3.1. What is “Temperature” in Nonequilibrium Steady States?

In most stages of our phenomenological construction of SST, the role of temperature has simply been to keep the environment constant.⁵¹ Therefore we did not have to be so careful about precise parameterization of the temperature. We simply used the same temperature scale as the heat baths, and declared that the temperature may be measured by a thermometer.

In the future development of SST, however, it is quite likely that we must examine the notion of temperature more carefully, and study the behavior of the SST entropy in a quantitative manner. We will face the problem to determine the temperature which is intrinsic to a nonequilibrium steady state. Let us discuss one possibility here.

We determined the V , N dependence of the free energy $F(T, v; V, N)$ in Sec. 6.1, using the pressure and the chemical potential. Both the quantities were determined operationally in Sec. 5 *without references to the value of the temperature*. The only requirement was that the temperature was fixed.

In Sec. 6.2, on the other hand, we discussed the formula (6.9) for density fluctuation. In this formula, the free energy appears in the dimensionless form $F/(k_B T)$. We have so far assumed simply that this T is the same temperature as the equilibrium temperature of the heat bath. (This is indeed the case in the driven lattice gas, See Sec. B.4.) But there is a possibility that this T should be replaced

⁵¹ The only exception is the definition (7.5) of the SST entropy, which involves a differentiation in T . But we did not have much quantitative discussions about the SST entropy.

by an “effective temperature” intrinsic to the nonequilibrium steady state, which may not necessarily be the same as the equilibrium temperature.

In other words, the fluctuation formula (6.9) may be used to experimentally determine the intrinsic nonequilibrium temperature since the free energy itself can be determined by other experiments which do not involve precise values of temperatures. Moreover, as we have discussed in Sec. 8.2.1, measurements related to linear response relations may be used to determine the nonequilibrium temperature directly.

From a theoretical point of view, the parameter β that appears in the formula (B.46) for the “weak canonicity” may be used to determine the nonequilibrium temperature of a stochastic model (which coincides with the usual temperature in the models studied in Appendix A.5).

8.3.2. *Don't Long-Range Correlations Destroy Thermodynamics?*

It is well-known that nonequilibrium steady states in a system with a conservation law generically exhibits spatial long range correlations.⁽²⁰⁾ More precisely correlation functions of some physical quantities decay slowly with a power law, even though the system is not at the critical point.

The mechanism of the long range correlation has been understood rather clearly from a phenomenological point of view, and the existence of long range correlations is confirmed in some experiments. There are also rigorous result⁽⁴⁰⁾ and explicit perturbative calculations^(44,81,92) which show that there indeed are such long range correlations in concrete stochastic models. No doubt the existence of long range spatial correlations is one of the intrinsic aspects of nonequilibrium steady states.

One might rather naively imagine that the existence of long range correlations is not consistent with the existence of thermodynamics since the correlations may destroy extensivity or locality. But of course this is far from the case. The best argument may be the fact (which will be rigorously established in Appendix) that we can construct perfectly consistent SST for the driven lattice gas, which is a typical model known to exhibit long range correlations. We do not only obtain general formulae for the thermodynamic functions but also compute them in the limit of high temperature and low density. We find nothing pathological that originates from the long range correlations.

The point is that the long range correlations show up (literally) in multi-point correlation functions, not in local observables. Thus they may lead to anomalous fluctuation of the sum of a certain quantity in a large region of the system. A notable example is anomalous density fluctuation mentioned in Sec. 6.2. If one looks at local quantities such as the pressure, the temperature or the density, on the other hand, one observes nothing anomalous originating from the long range

correlations. Thus all the thermodynamic quantities of SST, which are defined in terms of operations which involve local quantities, remain well-defined.

8.3.3. *Why do you Consider Walls and Contacts?*

The use of idealized walls and contacts may be the culture of thermodynamics. In conventional thermodynamics, one freely uses such devices as infinitely thin walls or perfectly adiabatic walls, or sometimes more delicate ones like semipermeable membrane.⁵² Decompositions, combinations, or contacts of various states realized by these walls play fundamental roles in the construction of thermodynamics. Of course boundaries are tricky objects even in equilibrium physics since properties of the system are inevitably modified near the boundaries. Nevertheless one can (very successfully) characterize bulk properties (not boundary properties) of equilibrium states by using all these walls and contacts. In many cases regions near boundaries are negligibly small compared with the bulk, and contacts are not modified by boundary effects.

Simply speaking, we wish to adopt the same strategy in our approach to nonequilibrium physics. We do consider various walls and contacts, but our main concern is to reveal universal properties exhibited by bulk of nonequilibrium steady states. Just as in equilibrium thermodynamics, walls and contacts are mere probes with which we investigate bulk properties.

Of course there is a possibility that one encounters various unexpected boundary effects caused by highly nonequilibrium nature of the states.⁵³ That is why we have carefully discussed the settings of the systems, the ways we insert and remove walls, the ways we put two systems into contact, and so on. We have tried to minimize unwanted disturbance of the states by the walls or contacts. Nevertheless there may still arise delicate material-dependent issues (like the temperature gap at boundaries) which complicate the analysis. In such cases, one should carefully distinguish such non-universal effects specific to boundaries from universal properties of the bulk, and try to minimize the former either theoretically or by experimentally devising a suitable setting. This may arouse nontrivial challenges for experimental designs, but we believe it is always possible in principle.

8.3.4. *Is SST Useful?*

If one assumes that SST is a correct theory describing nature, one can still ask if the theory is useful.

⁵² But see Ref. 3 for a severe criticism about the use of semipermeable membrane.

⁵³ A typical example is the delicateness about contact between nonequilibrium states and equilibrium states as discussed in Sec. 7.

To be honest, we admit that SST does not have much practical use at least in its present form. As we have mentioned in Sec. 1.3.1, for example, we cannot get any information about transport coefficients (linear or nonlinear) from the present form of SST. The present SST only deals with the response of a system at a fixed “degree of nonequilibrium.” As for the SST entropy, we do not expect it to play a significant role like its equilibrium counterpart. This is because we do not have (and do not expect to get) a natural operational definition of adiabatic operations for nonequilibrium systems. (But see Ref. 2 for an attempt.)

We believe that the significance of SST should be sought in more conceptual and theoretical aspects. First of all, the mere fact that there exists a consistent thermodynamics for a large class of nonequilibrium steady states (if true) must be regarded as news of fundamental importance. It shows that nonequilibrium states are not generated arbitrarily by time evolution, but are subject to a strict thermodynamic structure. More importantly from a practical point of view, establishment of thermodynamics can be a first important step toward a construction of statistical mechanics for steady states. We believe that such a statistical theory will not only of great theoretical interest but will have many practical applications.

APPENDIX A: WEAK CONTACT, DENSITY FLUCTUATION, AND LINEAR RESPONSE IN A SHEARED FLUID

In the present appendix, we discuss a particular scheme for making two subsystems of sheared fluid into contact, and examine some of the conjectures of SST. Analysis presented here is limited to the first and the second stages of SST (see Sec. 8.1), developed in Secs. 3 to 6, where we dealt with thermodynamics with a “fixed degree of nonequilibrium.” Based on some plausible assumptions, we can confirm our predictions about the density fluctuation stated in Sec. 6.2. We can go further to discuss linear response theory and a determination of the “nonequilibrium temperature.”

Compared with another “existence proof of SST” for the driven lattice gas presented in the next Appendix, the present approach is more heuristic. Nevertheless, the present setting has a clear advantage of being much closer to realistic systems. We hope that the results in the present Appendix and the next Appendix play complementary roles in reinforcing the logic of SST developed in the main body of the paper.

A.1. Weak Contact Scheme

Consider a system as in Fig. 19(a) in which a sheared fluid is separated into two parts by a horizontal wall. Both the lower and the upper parts have volume V and are characterized by the same “degree of nonequilibrium” (i.e., shear force)

τ . Following the strategy of Sec. 5.2, potential which is equal to u_1 and u_2 in the lower and the upper parts, respectively, is applied. We assume that the lower and the upper parts are separately in nonequilibrium steady states with densities ρ_1 and ρ_2 , respectively.

The horizontal wall has a window on it, which opens for a finite interval of time. We assume that the size of the window is much smaller than that of the wall, but is much larger than the molecular scale. Likewise the interval during which the window is open is much shorter than the relaxation time of macroscopic quantities, but is much longer than the molecular time scale. By j we denote the amount of fluid that passes through the window from the lower part to the upper part during the interval that the window is open.

After the window closes, we keep the system as it is for a sufficiently long time so that the two parts reach their steady states with the new densities $\rho'_1 = \rho_1 - (j/V)$, and $\rho'_2 = \rho_2 + (j/V)$, respectively.

We repeat many times the above procedure of (short) opening of the window followed by a (long) relaxation period. Then there takes place a very slow exchange of fluid between the lower and the upper parts of the system. This process of exchange may be described as a discrete time Markov process where the state is characterized by the densities (ρ_1, ρ_2) of the two parts. By analyzing this Markov process, we can examine the construction and the predictions of SST.

The main motivation for devising this weak contact is that nonequilibrium steady states generically develop spatial long-range correlations (see Sec. 8.3.2), which lead to anomalous density fluctuation and transport. Since our basic strategy in the present work (see Sec. 8.3.3) is to characterize the steady state in each system by examining the contact, the long range correlation *between* the two parts introduces unnecessary complication. By separating the two parts by a wall and allowing the exchange of fluid only via the small window during a finite interval, we can inhibit the system from developing long range correlations between the upper and the lower parts. (Of course long range correlation within each part is developed.)

Now we shall make some plausible assumptions about the behavior of the quantity j , the amount of fluid that have moved in a single opening. The most important assumption is that j is a random quantity whose behavior is determined solely by local properties of the nonequilibrium steady states at the both sides of the window. This is quite likely since the small window is open during the time interval which is much shorter than the relaxation time. An important consequence of this assumption is that the behavior of j essentially does not change when one increases the total volume V of the system (fixing the size and the opening interval of the window). This means that the change of the density in a single step, which is j/V , is proportional to V^{-1} . Thus j/V can be made much smaller than the change of the average density in response to a change of potential, and than the typical magnitude of the density fluctuation in a steady state (since the former change is

independent of V , and the latter fluctuation is proportional to $V^{-1/2}$). We shall make use of this smallness of j/V repeatedly in what follows.

To simplify the notation, we write the potential difference as $\Delta u = u_2 - u_1$, and write the densities in the lower and the upper parts as $\rho_1 = \rho_0 - \theta$ and $\rho_2 = \rho_0 + \theta$, respectively. Here ρ_0 is the total density, i.e., the total amount of fluid divided by the total volume. From now on we shall always describe the densities in the two parts using the deviation θ .

When Δu and θ are given, we denote by $\psi_{\Delta u, \theta}(j)$ the probability density for the variable j . We assume that $\psi_{\Delta u, \theta}(j)$ is independent of the volume V . We have omitted the dependence on T and τ since these variables are always fixed.

When $\Delta u = 0$ and $\theta = 0$, the two parts of the system are completely identical. Thus the corresponding probability density $\psi_{0,0}(j)$ is an even function of j with a peak at $j = 0$. We assume that $\psi_{0,0}(j)$ decays rapidly for large $|j|$, and is normalized as $\int dj \psi_{0,0}(j) = 1$.

When $\theta \neq 0$, i.e., when the densities become uneven, the probability density ψ becomes asymmetric. In the lowest order, this effect may be written as

$$\psi_{0,\theta}(j) \simeq \mathcal{N}(0, \theta) \psi_{0,0}(j) \exp[-\alpha_0 \theta j], \quad (\text{A.1})$$

where α_0 is a certain constant, and $\mathcal{N}(0, \theta)$ is the normalization constant. When there is a difference $\Delta u = u_2 - u_1$ in the potential, this is further modified as

$$\psi_{\Delta u, \theta}(j) \simeq \mathcal{N}(\Delta u, \theta) \psi_{0,0}(j) \exp\left[-\alpha_0 \theta j - \frac{\beta}{2} \Delta u j\right], \quad (\text{A.2})$$

again in the lowest order. Here β is a certain constant, which can of course be identified as an inverse (effective) temperature. Again the constant $\mathcal{N}(\Delta u, \theta)$ is chosen to ensure $\int dj \psi_{\Delta u, \theta}(j) = 1$.

A.2. Balance Condition and the Chemical Potential

Suppose that we apply a small potential difference $\Delta u = u_2 - u_1$ to the system, and repeat the process of opening the window sufficiently many times to have a steady balance between the lower and the upper parts. Since the balance is attained when $\psi_{\Delta u, \theta}(j)$ is symmetric in j , we get from (A.2) that

$$\alpha_0 \theta = -\frac{\beta}{2} \Delta u. \quad (\text{A.3})$$

Since the definition (5.3) of the chemical potential implies

$$\Delta u = u_2 - u_1 = \mu(\rho_0 - \theta) - \mu(\rho_0 + \theta) \simeq -2\theta \mu'(\rho_0), \quad (\text{A.4})$$

we can represent the derivative of the chemical potential as

$$\mu'(\rho_0) = \frac{\alpha_0}{\beta}. \quad (\text{A.5})$$

We note that when the two parts are in balance with each other, mechanical balance as we discussed in Sec. 5.3 also holds. This is because the window is sufficiently large and opens for a sufficiently long time for hydrodynamics to be efficient. Consequently, the chemical potential expressed as (A.5) satisfies the Maxwell relation (5.4) along with the pressure $p(\rho)$ defined from mechanical forces.

A.3. Density Fluctuation

We shall analyze the density fluctuation in the steady balance condition that we have characterized, and derive the conjectured Einstein's formula (6.9).

We fix the potential difference $\Delta u = u_2 - u_1$, and describe the densities in the lower and the upper parts as $\rho_1 = \rho_0 - \theta$ and $\rho_2 = \rho_0 + \theta$, respectively. From the balance condition (A.3), we see that the most probable value of the density deviation θ is given by

$$\theta_0 = -\frac{\beta \Delta u}{2 \alpha_0}. \quad (\text{A.6})$$

To describe the fluctuation around θ_0 , we denote by $p(\theta)$ the stationary probability density that densities in the two parts are $\rho_0 - \theta$ and $\rho_0 + \theta$, respectively. The stationary probability is the unique solution of

$$p(\theta) = \int d\theta' p(\theta') c(\theta' \rightarrow \theta), \quad (\text{A.7})$$

for any θ , where

$$c\left(\theta \rightarrow \theta + \frac{j}{V}\right) = V \psi_{\Delta u, \theta}(j) \quad (\text{A.8})$$

is the transition probability density. It is normalized as

$$\int d\theta' c(\theta \rightarrow \theta') = 1. \quad (\text{A.9})$$

The condition (A.7) is the continuous state-variable version of (2.24).

As we shall see below, the solution of (A.7) can be obtained by assuming the detailed balance condition (see Sec. 2.3.2)

$$p(\theta) c(\theta \rightarrow \theta') = p(\theta') c(\theta' \rightarrow \theta), \quad (\text{A.10})$$

for any θ and θ' . Clearly (A.10) along with (A.9) implies (A.7), but not vice versa.

If we substitute $\theta' = \theta + (j/V)$, (A.8), and (A.2), the detailed balance condition (A.10) becomes

$$\begin{aligned} & p(\theta) \mathcal{N}(\Delta u, \theta) \exp\left[-\alpha_0 \theta j - \frac{\beta}{2} \Delta u j\right] \\ &= p\left(\theta + \frac{j}{V}\right) \mathcal{N}\left(\Delta u, \theta + \frac{j}{V}\right) \left[\alpha_0 \left(\theta + \frac{j}{V}\right) j + \frac{\beta}{2} \Delta u j\right] \end{aligned} \quad (\text{A.11})$$

We then have

$$\frac{p(\theta)}{p(\theta + (j/V))} \simeq \exp[2\alpha_o \theta j + \beta \Delta u j], \tag{A.12}$$

where we have used the smallness of j/V to neglect j^2/V in the exponential and set $\mathcal{N}(\Delta u, \theta + (j/V))/\mathcal{N}(\Delta u, \theta) \simeq 1$. By taking the logarithm and again noting that j/V is small, we get

$$-\frac{j}{V} \frac{\partial}{\partial \theta} \log p(\theta) \simeq 2\alpha_o \theta j + \beta \Delta u j, \tag{A.13}$$

which can readily be solved to give

$$p(\theta) \propto \exp[-\alpha_o V (\theta - \theta_0)^2] = \exp\left[-\beta \mu'(\rho_0) \frac{(\Delta N)^2}{V}\right] \tag{A.14}$$

where $\Delta N = (\theta - \theta_0) V$ is the deviation measured by the amount of fluid. This is nothing but the Einstein's formula (6.9), expanded to the lowest order in ΔN .

A.4. Linear Transport

We finally treat time-dependent linear transport through the weak contact, and prove the corresponding fluctuation-response relation. This is especially useful since the resulting relations can be used to determine the parameter β in (A.2) by using measurable quantities. See Sec. A.5.

It may appear surprising that one can deal with transport phenomena in a highly nonequilibrium system. In this case, however, we are dealing with a very weak flow in the direction orthogonal to the (strong) shear flow. This enables us to treat the transport by using only elementary techniques in Markov processes.

Suppose, for simplicity, that the two parts have been in a steady contact with vanishing potential difference $\Delta u = u_2 - u_1 = 0$. At an instant, we apply a nonvanishing but small potential difference⁵⁴ Δu . Then there takes place a relaxation from a nonequilibrium steady state with $\Delta u = 0$ to another nonequilibrium steady state with nonvanishing Δu .

Let us define the single-step time evolution operator by

$$[\hat{T}_{\Delta u} p](\theta) = \int d\theta' p(\theta') c_{\Delta u}(\theta' \rightarrow \theta), \tag{A.15}$$

where we have explicitly labeled $c(\theta \rightarrow \theta')$ (defined in (A.8)) with the potential difference Δu . The probability density after M openings of the window is given by

$$p_M(\theta) = [(\hat{T}_{\Delta u})^M p_0](\theta), \tag{A.16}$$

⁵⁴It is also easy to treat time-dependent perturbation as we shall do in Sec. B.6.

where $p_0(\theta)$ is the stationary distribution for the case $\Delta u = 0$.

We wish to express $\hat{T}_{\Delta u}$ as a perturbation to \hat{T}_0 . As for the transition probability, we find from (A.8) and (A.2) that

$$\begin{aligned} c_{\Delta u}(\theta' \rightarrow \theta) &= \frac{\mathcal{N}(\Delta u, \theta')}{\mathcal{N}(0, \theta')} \exp \left[-\frac{\beta}{2} \Delta u (\theta - \theta') V \right] c_0(\theta' \rightarrow \theta) \\ &= c_0(\theta' \rightarrow \theta) - \frac{\beta}{2} \Delta u (\theta - \theta') V c_0(\theta' \rightarrow \theta) \\ &\quad + \frac{\beta}{2} \Delta u \int d\theta'' (\theta'' - \theta') V c_0(\theta' \rightarrow \theta'') + O((\Delta u)^2) \end{aligned} \quad (\text{A.17})$$

where the contribution from the normalization factor has been determined by noting that $\int d\theta c_0(\theta' \rightarrow \theta) = \int d\theta c_{\Delta u}(\theta' \rightarrow \theta) = 1$. To proceed we need to work on the third term in the right-hand side of (A.17). By writing $\theta'' = \theta' + (j/V)$, the relevant integral becomes

$$\begin{aligned} \int d\theta'' (\theta'' - \theta') V c_0(\theta' \rightarrow \theta'') &= \frac{1}{V} \int dj j c_0 \left(\theta' \rightarrow \theta' + \frac{j}{V} \right) \\ &\simeq - \left(\alpha_0 \theta' + \frac{\beta}{2} \Delta u \right) (j_0)^2, \end{aligned} \quad (\text{A.18})$$

where the final approximate expression is obtained from (A.8), (A.2), and a new (but plausible) assumption that $\psi_{0,0}(j) \propto \exp(-j^2/\{2(j_0)^2\})$. Here $j_0 > 0$ is the typical value for the quantity j . We now note that θ and θ' differ only by $O(j_0/V)$. Therefore (A.18) implies that one can replace θ' by θ as

$$\begin{aligned} \int d\theta'' (\theta'' - \theta') V c_0(\theta' \rightarrow \theta'') &= \int d\theta'' (\theta'' - \theta) V c_0(\theta \rightarrow \theta'') \\ &\quad + O \left(\frac{\alpha_0 (j_0)^3}{V} \right), \end{aligned} \quad (\text{A.19})$$

where the difference is so small for large systems that we shall neglect it from now on. By substituting the replacement (A.19) into (A.17), we have

$$\begin{aligned} c_{\Delta u}(\theta' \rightarrow \theta) &= c_0(\theta' \rightarrow \theta) - \frac{\beta}{2} \Delta u (\theta - \theta') V c_0(\theta' \rightarrow \theta) \\ &\quad + \frac{\beta}{2} \Delta u \int d\theta'' (\theta'' - \theta) V c_0(\theta \rightarrow \theta'') + O((\Delta u)^2). \end{aligned} \quad (\text{A.20})$$

By substituting (A.20) into (A.15), we get

$$[\hat{T}_{\Delta u} p](\theta) \simeq [\hat{T}_0 p](\theta) - \frac{\beta \Delta u}{2} \int d\theta' (\theta - \theta') V \{p(\theta') c_0(\theta' \rightarrow \theta)\}$$

$$+ p(\theta) c_0(\theta \rightarrow \theta')\}. \quad (\text{A.21})$$

When applied to $p_0(\theta)$, the stationary condition $[\hat{T}_0 p_0](\theta) = p_0(\theta)$ and the detailed balance condition (A.10) makes the expression (A.21) much simpler as

$$\begin{aligned} [\hat{T}_{\Delta u} p_0](\theta) &\simeq p_0(\theta) - \beta \Delta u \int d\theta' (\theta - \theta') V p_0(\theta') c_0(\theta' \rightarrow \theta) \\ &= p_0(\theta) - \beta \Delta u [\hat{j} p_0](\theta) \end{aligned} \quad (\text{A.22})$$

We have defined the operator \hat{j} by

$$[\hat{j} p](\theta) = \int d\theta' (\theta - \theta') V p(\theta') c_0(\theta' \rightarrow \theta), \quad (\text{A.23})$$

which counts the total amount of the fluid that have moved and at the same time generates a single-step time evolution.

By substituting (A.22) into (A.16), and expanding in Δu , we find

$$p_M(\theta) = p_0(\theta) - \beta \Delta u \sum_{m=0}^{M-1} [(\hat{T}_0)^m \hat{j} p_0](\theta) + O((\Delta u)^2). \quad (\text{A.24})$$

This is our basic equation for the linear response theory.

Let $N_1(\theta) = (\rho_0 - \theta) V$ be the total amount of fluid in the lower part. We denote its average after M openings of the window as $\langle \hat{N}_1(M) \rangle_{\Delta u} = \int d\theta N_1(\theta) p_M(\theta)$. Here $\langle \hat{N}_1(M) \rangle_{\Delta u}$, as a function of M , describes the relaxation phenomenon after the potential difference Δu was turned on. By using (A.24), we find that

$$\begin{aligned} \langle \hat{N}_1(M) \rangle_{\Delta u} &= N_0 - \beta \Delta u \sum_{m=0}^{M-1} N_1(\theta) [(\hat{T}_0)^m \hat{j} p_0](\theta) + O((\Delta u)^2) \\ &= N_0 - \beta \Delta u \sum_{m=0}^{M-1} \langle \hat{N}_1(M) \hat{j}(M-m) \rangle_0 + O((\Delta u)^2), \end{aligned} \quad (\text{A.25})$$

where $N_0 = V \rho_0 = \int d\theta N_1(\theta) p_0(\theta)$ is the amount of fluid in the lower part in the steady state with $\Delta u = u_1 - u_2 = 0$. The definition of the temporal correlation function $\langle \hat{N}_1(M) \hat{j}(M-m) \rangle_0$ can be read off from (A.25).

Reflecting the fact that \hat{j} measures the amount of fluid moved from the lower to the upper part, (A.25) can be further rewritten in the form

$$\langle \hat{N}_1(M) \rangle_{\Delta u} = N_0 + \beta \Delta u \langle \hat{N}_1(M) \{ \hat{N}_1(M) - \hat{N}_1(0) \} \rangle_0 + O((\Delta u)^2). \quad (\text{A.26})$$

Thus the relaxation phenomenon is fully described (in the lowest order in Δu) in terms of the temporal correlation function in the steady state without a potential difference. This means that one can unambiguously

determine the inverse temperature β by measuring the behavior of the variable N_1 .

A.5. Discussion

In the present appendix, we have devised a weak contact realized by a small window in the setting of a sheared fluid. Based on plausible assumptions about the exchange of fluid through the window, we were able to recover the conjecture of SST about the density fluctuation. We were further able to show the fluctuation-response relation for the time-dependent relaxation phenomena.

It is crucial that we have discussed three different settings and the corresponding measurements, namely, to measure i) the most probable densities when a potential difference is applied (Sec. A.2), ii) the density fluctuation for a fixed potential difference (Sec. A.3), and iii) the relaxation phenomena (Sec. A.4) when a potential difference is suddenly applied.

From i), we get information about $\mu'(\rho)$, and, from ii), we get $\beta \mu'(\rho)$. These two already give nontrivial prediction to experimental results provided that the parameter β can be identified as the inverse temperature. This is what we expect most naively, but there is a possibility that β should be regarded as the nonequilibrium inverse temperature which deviates slightly from its equilibrium counterpart (see Sec. 8.3.1). In such a case, iii) provides a definite operational method for measuring the “nonequilibrium inverse temperature” β . Thus the three measurements proposed in i), ii), and iii) together form a complete operational test about the validity of (a part of) SST.

It is quite interesting whether the present weak contact scheme can be applied to systems other than the sheared fluid. Strictly speaking the present argument works when there is a symmetry between the two parts. Thus it can be applied directly only to systems with a symmetry such as the $(T, \phi; V, N)$ formalism of electrically conducting fluid. It would be very useful if similar scheme can be developed in more general systems. Needless to say, a major remaining challenge is to devise similar realization of the μ -wall contact that we have discussed in Sec.7. For the moment this problem seems quite delicate, and we have concrete results only in the driven lattice gas (see Sec. B.7).

APPENDIX B: SST IN THE DRIVEN LATTICE GAS

In the main body of the paper, we have developed the framework of steady state thermodynamics (SST) from a macroscopic phenomenological point of view. In the present Appendix, we will develop a microscopic point of view, and

demonstrate that SST can be realized in nonequilibrium steady states of a standard Markov process called the driven lattice gas. This provides a complementary analysis to the “mesoscopic” approach developed in the Appendix B.3.4. The argument here is quite general and can be extended to a much larger class of Markov processes.

With this “existence proof” we can be sure that our framework of SST is theoretically consistent. Moreover concrete mathematical results in the driven lattice gas may give us hints for further development of our phenomenology.

Here we introduce the driven lattice gas, and realize a weak contact to determine the chemical potential, the pressure, and the free energy. We get general formulae for these thermodynamic quantities, which allow us to compute them explicitly (by using, for example, a computer or a systematic expansion). We also present results of the simplest calculation in the limit of high temperature and low density.

We stress that we are *not* defining these thermodynamic quantities based on formal analogies with the equilibrium statistical mechanics, but rather defining everything based on the operational procedures discussed carefully in Sec.5. Therefore our free energy F is (at least for the moment) not related to a statistical quantity through a relation like $F = -(1/\beta) \log Z$ or $S = k_B \log \mathcal{W}$.

We also show that the fluctuation relation (see Sec. 6.2) and the minimum work principle (see Sec. 6.3) hold exactly in these models. We argue that an ideal μ -wall (see Sec.7.2) may be constructed for the driven lattice gas. We can go further to develop a linear response theory for time-dependent particle exchange process through weak coupling (see Sec.A.4).

As is clear from the summary in the above paragraphs, we can reproduce most aspects of our phenomenological construction.

Remark: If one applies the construction in the present Appendix to a Markov process whose stationary distribution corresponds to an equilibrium state, then we get thermodynamic quantities which exactly coincide with those obtained from equilibrium statistical mechanics. This fact alone is of some interest since our derivation involves only local correlation functions, nothing analogous to the partition function. One may regard our construction as a robust method of “getting thermodynamics without a partition function,” which can be applied to nonequilibrium steady states as well as equilibrium states.

B.1. Definition

Let us define the driven lattice gas. It belongs to a class of models which are obtained by making minimum modifications to Markov processes for equilibrium dynamics discussed in Sec. 2.3. As we have stressed in Sec. 2.3.2, the detailed balance condition (2.25) with respect to the equilibrium state is a fundamental

requirement for constructing physically meaningful models for equilibrium dynamics. Unfortunately we still do not know what are corresponding guiding principles in nonequilibrium stochastic dynamics. This means that we must proceed carefully, not over-trusting results from model studies, and always questioning robustness of conclusions.

For simplicity we treat models in two dimensions, but extensions to higher dimensions are automatic. Define an $\ell \times h$ lattice Λ by

$$\Lambda = \left\{ \mathbf{x} = (x_1, x_2) \mid x_1 = 0, \pm 1, \dots, \pm \frac{\ell-1}{2}, x_2 = 0, \pm 1, \dots, \pm \frac{h-1}{2} \right\}, \quad (\text{B.1})$$

where (as usual) x_1 and x_2 are the horizontal and the vertical coordinates, respectively. Lattice sites are denoted as $\mathbf{x}, \mathbf{y}, \dots \in \Lambda$. We impose periodic boundary conditions (i.e., we identify $x_1 = (\ell+1)/2$ with $x_1 = -(\ell-1)/2$, and $x_2 = (h+1)/2$ with $x_2 = -(h-1)/2$). For each site $\mathbf{x} \in \Lambda$, we associate an occupation variable $\eta_{\mathbf{x}}$. We set $\eta_{\mathbf{x}} = 1$ if the site \mathbf{x} is occupied by a particle, and $\eta_{\mathbf{x}} = 0$ if \mathbf{x} is empty. We do not allow more than two particles to occupy a single site. See Fig. 20.

We denote a collection of $\eta_{\mathbf{x}}$ for all $\mathbf{x} \in \Lambda$ as

$$\boldsymbol{\eta} = (\eta_{\mathbf{x}})_{\mathbf{x} \in \Lambda}, \quad (\text{B.2})$$

and call it a *configuration*. A configuration $\boldsymbol{\eta}$ corresponds to a microscopic state s in Secs. 2.2 and 2.3. For a given configuration $\boldsymbol{\eta}$, we write

$$|\boldsymbol{\eta}| = \sum_{\mathbf{x} \in \Lambda} \eta_{\mathbf{x}}, \quad (\text{B.3})$$

which is the total number of particles in $\boldsymbol{\eta}$.

The Hamiltonian $H_{\Lambda}(\cdot)$ gives the energy $H_{\Lambda}(\boldsymbol{\eta})$ for a configuration $\boldsymbol{\eta}$ on the lattice Λ . Although our discussion does not depend on the specific choice of $H_{\Lambda}(\cdot)$

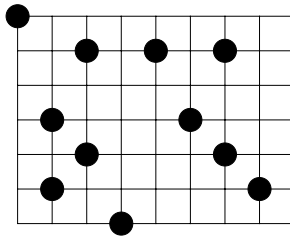


Fig. 20. Basic setup of lattice gas models. Particles live on sites of the $\ell \times h$ two dimensional lattice. Particles hop around the lattice according to given transition rates.

(except in Sec. B.8), let us take for concreteness the Ising Hamiltonian

$$H_{\Lambda}(\boldsymbol{\eta}) = -J \sum_{\langle x,y \rangle} \eta_x \eta_y, \quad (\text{B.4})$$

where J is the coupling constant, and the sum is over all pairs of nearest neighbor sites (according to the periodic boundary conditions). Although the symbol J is used to denote the flux in the main body of the paper, we here follow the standard notation in the driven lattice gas.

For a site $\mathbf{x} \in \Lambda$ and a configuration $\boldsymbol{\eta}$, we denote by $\boldsymbol{\eta}^{\mathbf{x}}$ the new configuration obtained by changing⁵⁵ the value of $\eta_{\mathbf{x}}$ in $\boldsymbol{\eta}$. More precisely, we set

$$(\boldsymbol{\eta}^{\mathbf{x}})_y = \begin{cases} 1 - \eta_x & \text{if } y = \mathbf{x}; \\ \eta_y & \text{if } y \neq \mathbf{x}. \end{cases} \quad (\text{B.5})$$

Similarly for $\mathbf{x}, \mathbf{y} \in \Lambda$ and a configuration $\boldsymbol{\eta}$, we denote by $\boldsymbol{\eta}^{\mathbf{x},\mathbf{y}}$ the configuration obtained by changing both $\eta_{\mathbf{x}}$ and $\eta_{\mathbf{y}}$.

We can define a Markov process using the general discussion in Sec. 2.3.1 once we specify the transition rates $c_{\Lambda}^{(T,E)}(\boldsymbol{\eta} \rightarrow \boldsymbol{\eta}')$. For any configuration $\boldsymbol{\eta}$ and any $\mathbf{x}, \mathbf{y} \in \Lambda$ such that $|\mathbf{x} - \mathbf{y}| = 1$, we set

$$\begin{aligned} c_{\Lambda}^{(T,E)}(\boldsymbol{\eta} \rightarrow \boldsymbol{\eta}^{\mathbf{x},\mathbf{y}}) &= \eta_{\mathbf{x}}(1 - \eta_{\mathbf{y}}) \phi[\beta\{H_{\Lambda}(\boldsymbol{\eta}^{\mathbf{x},\mathbf{y}}) - H_{\Lambda}(\boldsymbol{\eta}) + E(x_1 - y_1)\}] \\ &\quad + (1 - \eta_{\mathbf{x}})\eta_{\mathbf{y}} \phi[\beta\{H_{\Lambda}(\boldsymbol{\eta}^{\mathbf{x},\mathbf{y}}) - H_{\Lambda}(\boldsymbol{\eta}) + E(y_1 - x_1)\}], \end{aligned} \quad (\text{B.6})$$

where $\beta = 1/(k_B T)$ is the inverse temperature and E is the “electric field” in the x_1 direction. Here $\phi(h)$ is the function introduced in Sec. 2.3.1, and again satisfies (2.28). The first term in the transition rate (B.6) represents a hop of particle from \mathbf{x} to \mathbf{y} and the second term from \mathbf{y} to \mathbf{x} . We set $c_{\Lambda}^{(T,E)}(\boldsymbol{\eta} \rightarrow \boldsymbol{\eta}') = 0$ for $\boldsymbol{\eta}, \boldsymbol{\eta}'$ not of the form (B.6). Note that the particle number $|\boldsymbol{\eta}|$ is conserved in the allowed transitions.

A Markov process with the transition rates (B.6) is ergodic (see Sec. 2.3.1) in a state space with a fixed $|\boldsymbol{\eta}|$. Thus for each positive integer $N \leq \ell h$, there is a unique stationary distribution $p_{\Lambda,N}^{(T,E)}(\boldsymbol{\eta})$ which is nonvanishing only when $|\boldsymbol{\eta}| = N$. When $E \neq 0$, this stationary distribution represents the nonequilibrium steady state of the system. We denote the average over the steady state distribution as

$$\langle g(\boldsymbol{\eta}) \rangle_{\Lambda,N}^{(T,E)} = \sum_{\boldsymbol{\eta}} g(\boldsymbol{\eta}) p_{\Lambda,N}^{(T,E)}(\boldsymbol{\eta}), \quad (\text{B.7})$$

where $g(\boldsymbol{\eta})$ is an arbitrary function of configurations.

⁵⁵ Since $\eta_{\mathbf{x}} = 0, 1$, the change means $0 \rightarrow 1$ or $1 \rightarrow 0$.

In the steady state of the present driven lattice gas, there is a constant flow of particles toward the right. In this sense the model has some resemblance with the $(T, \phi; V, N)$ formalism of electrical conduction. See Sec.4.4, especially Fig. 13(b). Note that we do not have electric plates here, which are effectively replaced by the periodic boundary conditions. Since the parameter E corresponds to electric field, we can identify the nonequilibrium intensive variable as $\phi = E\ell$. For convenience, however, we shall use the parameter E (which may also be regarded as an intensive nonequilibrium variable) to characterize the steady states.

B.2. Local Detailed Balance Condition

Take any $\mathbf{x}, \mathbf{y} \in \Lambda$ such that $|\mathbf{x} - \mathbf{y}| = 1$, and let $\boldsymbol{\eta}$ be any configuration such that $\eta_{\mathbf{x}} = 1$ and $\eta_{\mathbf{y}} = 0$. Then the definition (B.6) and the condition (2.28) for $\phi(h)$ implies

$$\frac{c_{\Lambda}^{(T,E)}(\boldsymbol{\eta} \rightarrow \boldsymbol{\eta}^{\mathbf{x},\mathbf{y}})}{c_{\Lambda}^{(T,E)}(\boldsymbol{\eta}^{\mathbf{x},\mathbf{y}} \rightarrow \boldsymbol{\eta})} = \exp[\beta\{H_{\Lambda}(\boldsymbol{\eta}) - H_{\Lambda}(\boldsymbol{\eta}^{\mathbf{x},\mathbf{y}}) + E(y_1 - x_1)\}], \quad (\text{B.8})$$

which should be compared with the detailed balance condition (2.26) in equilibrium dynamics. It must be noted that there is no single function⁵⁶ $\tilde{H}(\cdot)$ which enables us to express the right-hand side of (B.8) simply as $\exp[\{\tilde{H}(\boldsymbol{\eta}) - \tilde{H}(\boldsymbol{\eta}^{\mathbf{x},\mathbf{y}})\}]$. Try, for example, $\tilde{H}(\boldsymbol{\eta}) = H_{\Lambda}(\boldsymbol{\eta}) - E \sum_{\mathbf{x} \in \Lambda} x_1 \eta_{\mathbf{x}}$. Then (B.8) is equal to $\exp[\beta\{\tilde{H}(\boldsymbol{\eta}) - \tilde{H}(\boldsymbol{\eta}^{\mathbf{x},\mathbf{y}})\}]$ for most \mathbf{x} except for those at boundaries. For any $\mathbf{x} \in \Lambda$ one can choose a $\tilde{H}(\cdot)$ which covers sites around \mathbf{x} , but not the whole lattice. In this sense, the relation (B.8) is sometimes called⁵⁷ the ‘‘local detailed balance.’’

B.3. Determination of Thermodynamic Quantities

We will see how we can realize the weak contact of two systems, and evaluate thermodynamic quantities.

B.3.1. Weak contact in Lattice Gases

We shall now realize in the context of lattice gases the idea of weak contact.

⁵⁶ If there was one, we could write the steady state distribution as $p_{\text{ss}}(\boldsymbol{\eta}) = \tilde{Z}^{-1} \exp[-\beta\tilde{H}(\boldsymbol{\eta})]$, and the Markov process would satisfy the detailed balance condition with respect to $p_{\text{ss}}(\boldsymbol{\eta})$.

⁵⁷ The term ‘‘local detailed balance’’ might be a bit confusing. A detailed balance condition, as in (2.25), is always stated with respect to a particular stationary distribution. Here one still does not know what the stationary distribution is. A condition like (B.8) may be better called ‘‘local energy conservation.’’

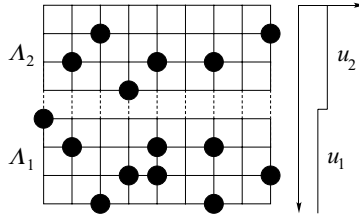


Fig. 21. Weak contact of two steady states in a lattice gas model. Potential which is equal to u_1 and u_2 on the lattices Λ_1 and Λ_2 , respectively, is applied to the system. The potential only modifies the transition rates between the two lattices. By using this setting we can define the chemical potential of a lattice gas model. In fact the same setting can be used to realize a perfect μ -wall that connects a nonequilibrium steady state with an equilibrium state. See Sec. B.7.

Let Λ_1 and Λ_2 be $\ell \times h$ lattices identical to Λ of (B.1). (It is automatic to extend the present discussion to cases where Λ_1 and Λ_2 are not identical.) We denote by η and ζ lattice gas configurations on Λ_1 and Λ_2 , respectively. The total Hamiltonian is

$$H_{\text{tot}}^{(u_1, u_2)}(\eta, \zeta) = H_{\Lambda_1}(\eta) + H_{\Lambda_2}(\zeta) + u_1|\eta| + u_2|\zeta|, \quad (\text{B.9})$$

where $H_{\Lambda_i}(\cdot)$ ($i = 1, 2$) are copies of the Hamiltonian $H_{\Lambda}(\cdot)$, and u_1 and u_2 are uniform potentials applied to Λ_1 and Λ_2 , respectively. Note that such a potential does not affect the dynamics within Λ_1 or Λ_2 at all, and only modifies hopping between the two lattices (See Fig. 21).

Our Markov process is defined by the transition rates $c_{\Lambda_1}^{(T, E)}(\eta \rightarrow \eta^{x, y})$ and $c_{\Lambda_2}^{(T, E)}(\zeta \rightarrow \zeta^{x, y})$ (which are faithful copies of $c_{\Lambda}^{(T, E)}(\eta \rightarrow \eta^{x, y})$ of (B.6)) within each sublattice, and additional transition rates for hops between the two sublattices Λ_1 and Λ_2 .

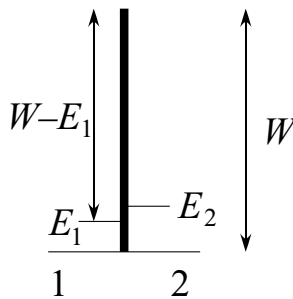


Fig. 22. A system consisting of two states 1 and 2 which are separated by a large energy barrier W . By examining equilibrium dynamics that satisfies the detailed balance condition, we can determine the transition rates $c(1 \rightarrow 2)$ and $c(2 \rightarrow 1)$.

Let us pose here and examine how one should design transition rates for two subsystems that are coupled very weakly. Here we assume that the weak coupling is realized by the presence of a very large energy barrier for transitions between the two subsystems. For simplicity let us first consider a system with two states 1 and 2 with the energies E_1 and E_2 , and assume that the two states are separated by an energy barrier $W \gg E_1, E_2$. See Fig. 22. We shall construct a Markov process describing the equilibrium of this system. Suppose that the system is in the state 1. In order for the system to jump into the state 2, it must first reach the top of the energy barrier, raising the energy by $W - E_1$. Since there is no cost required for falling down into the state 2, we may assume that the transition rate from the state 1 to 2 is fully determined by the relative height $W - E_1$ of the wall. This means that we can write $c(1 \rightarrow 2) = \psi(W - E_1)$ with some function $\psi(h)$. Similarly we have $c(2 \rightarrow 1) = \psi(W - E_2)$ for the opposite transition. By requiring the detailed balance condition (2.26)

$$\frac{c(1 \rightarrow 2)}{c(2 \rightarrow 1)} = \frac{\psi(W - E_1)}{\psi(W - E_2)} = e^{\beta(E_1 - E_2)}, \quad (\text{B.10})$$

we find that the only possible choice is $\psi(h) = c e^{-\beta h}$ with some constant c . Thus we find that

$$c(1 \rightarrow 2) = \varepsilon e^{\beta E_1}, \quad c(2 \rightarrow 1) = \varepsilon e^{\beta E_2}, \quad (\text{B.11})$$

with $\varepsilon = c e^{-\beta W}$. Note that the assumption of very high energy barrier led us to the essentially unique choice of the transition rates.⁵⁸

Now we come back to the task of realizing a weak contact between two sublattices of driven lattice gas defined on Λ_1 and Λ_2 . We assume that, for each $j = 0, \pm 1, \dots, \pm(\ell - 1)/2$, a particle can hop between the site⁵⁹ $(j, 0)$ in Λ_1 and the corresponding site $(j, 0)$ in Λ_2 . We also assume that the particle must go over a very high energy barrier to execute such a hop. Then we see that the transition rates should be of the form (B.11), where E_1, E_2 should be interpreted as local energies. Then we get⁶⁰

$$\begin{aligned} c[(\boldsymbol{\eta}, \boldsymbol{\zeta}) \rightarrow (\boldsymbol{\eta}^x, \boldsymbol{\zeta}^x)] &= \varepsilon \eta_x (1 - \zeta_x) \exp[\beta\{H_{\Lambda_1}(\boldsymbol{\eta}) - H_{\Lambda_1}(\boldsymbol{\eta}^x) + u_1\}] \\ &\quad + \varepsilon (1 - \eta_x) \zeta_x \exp[\beta\{H_{\Lambda_2}(\boldsymbol{\zeta}) - H_{\Lambda_2}(\boldsymbol{\zeta}^x) + u_2\}], \end{aligned} \quad (\text{B.12})$$

⁵⁸ Also note that the rates used here do *not* fit into the general form assumed in Sec. 2.3.1.

⁵⁹ Note that both the sites are in the bulk of each subsystem since we impose periodic boundary conditions. We have chosen this definition since our main purpose is to characterize bulk properties of nonequilibrium steady states rather than to investigate properties of realistic contact. See Sec. 8.3.3. In equilibrium, the second law guarantees that it does not make any difference (in macroscopic scale) whether one puts boundary sites or bulk sites into contact. We still do not know whether nonequilibrium steady states possess similar robustness.

⁶⁰ Going back to the definition (B.5) of $\boldsymbol{\eta}^x$, one sees immediately that the values (which can be 0 or 1) of η_x and ζ_x are simply exchanged in the process $(\boldsymbol{\eta}, \boldsymbol{\zeta}) \rightarrow (\boldsymbol{\eta}^x, \boldsymbol{\zeta}^x)$, no matter what $\boldsymbol{\eta}$ and $\boldsymbol{\zeta}$ are.

for $\mathbf{x} = (j, 0)$ with $j = 0, \pm 1, \dots, \pm(\ell - 1)/2$. We set $c[(\boldsymbol{\eta}, \boldsymbol{\zeta}) \rightarrow (\boldsymbol{\eta}', \boldsymbol{\zeta}')] = 0$ for configurations not of the form (B.12). The first term in (B.12) represents a hop from Λ_1 to Λ_2 and the second term from Λ_2 to Λ_1 . Note that we do not have terms involving the electric field E in (B.12) since we imagine that particles hop in the direction orthogonal to the field. Indeed for any nonvanishing $c[(\boldsymbol{\eta}, \boldsymbol{\zeta}) \rightarrow (\boldsymbol{\eta}^x, \boldsymbol{\zeta}^x)]$ we have the detailed balance condition (see (2.26))

$$\frac{c[(\boldsymbol{\eta}, \boldsymbol{\zeta}) \rightarrow (\boldsymbol{\eta}^x, \boldsymbol{\zeta}^x)]}{c[(\boldsymbol{\eta}^x, \boldsymbol{\zeta}^x) \rightarrow (\boldsymbol{\eta}, \boldsymbol{\zeta})]} = \exp[\beta\{H_{\text{tot}}^{(u_1, u_2)}(\boldsymbol{\eta}, \boldsymbol{\zeta}) - H_{\text{tot}}^{(u_1, u_2)}(\boldsymbol{\eta}^x, \boldsymbol{\zeta}^x)\}]. \quad (\text{B.13})$$

We investigate the steady state of this model with the total particle number $|\boldsymbol{\eta}| + |\boldsymbol{\zeta}| = 2N$ where N is a constant. When $\varepsilon = 0$, the two sublattices decouple, and hence the distribution $p_{\Lambda_1, N_1}^{(T, E)}(\boldsymbol{\eta}) p_{\Lambda_2, N_2}^{(T, E)}(\boldsymbol{\zeta})$ with any fixed N_1, N_2 such that $N_1 + N_2 = 2N$ is stationary. We want to see how this situation is modified in the lowest order of $\varepsilon > 0$.

In the limit $\varepsilon \rightarrow 0$, where particle exchanges between Λ_1 and Λ_2 are infinitesimally rare, the states within Λ_1 and Λ_2 first reach their steady states. When a particle hops between Λ_1 and Λ_2 , again the states in the two sublattices relax to the steady states with the new particle numbers. Such a separation of time scale enables us to study stochastic dynamics of particle exchange between Λ_1 and Λ_2 separately from the relaxation process in each sublattice.

We fix the total particle number $2N$, and denote by N_1 the number of particles in Λ_1 . Since the number of particles in Λ_2 is automatically known to be $N_2 = 2N - N_1$, we only specify N_1 in what follows. Since a hop between the two sublattices takes place in the distribution $p_{\Lambda_1, N_1}^{(T, v)}(\boldsymbol{\eta}) p_{\Lambda_2, N_2}^{(T, v)}(\boldsymbol{\zeta})$, the effective transition rate for a hop from Λ_1 to Λ_2 is obtained by averaging the sum of the rates (B.12) as

$$\begin{aligned} & \tilde{c}(N_1 \rightarrow N_1 - 1) \\ &= \left\langle \sum_{j=-(\ell-1)/2}^{(\ell-1)/2} \eta_{(j,0)} (1 - \zeta_{(j,0)}) c[(\boldsymbol{\eta}, \boldsymbol{\zeta}) \rightarrow (\boldsymbol{\eta}^{(j,0)}, \boldsymbol{\zeta}^{(j,0)})] \right\rangle_{\Lambda_1, N_1; \Lambda_2, N_2}^{(T, E)} \\ &= \varepsilon \sum_{j=-(\ell-1)/2}^{(\ell-1)/2} \langle \eta_{(j,0)} (1 - \zeta_{(j,0)}) \exp[\beta\{H_{\Lambda_1}(\boldsymbol{\eta}) \\ & \quad - H_{\Lambda_1}(\boldsymbol{\eta}^{(j,0)}) + u_1\}] \rangle_{\Lambda_1, N_1; \Lambda_2, N_2}^{(T, E)}, \end{aligned} \quad (\text{B.14})$$

where the average is taken over $p_{\Lambda_1, N_1}^{(T, E)}(\boldsymbol{\eta}) p_{\Lambda_2, N_2}^{(T, E)}(\boldsymbol{\zeta})$. By noting that the average separates into those for each sublattice, and using the translation invariance, we

find

$$\tilde{c}(N_1 \rightarrow N_1 - 1) = \varepsilon \ell \left(1 - \frac{N_2}{V}\right) g(N_1) e^{\beta u_1}, \quad (\text{B.15})$$

where $V = \ell h$ and

$$\begin{aligned} g(N) &= \langle \eta_{\mathbf{x}} \exp[\beta\{H_{\Lambda}(\boldsymbol{\eta}) - H_{\Lambda}(\boldsymbol{\eta}^{\mathbf{x}})\}] \rangle_{\Lambda, N}^{(T, E)} \\ &= \left\langle \eta_{\mathbf{x}} \exp\left[-\beta J \sum_{\mathbf{y}:|\mathbf{y}-\mathbf{x}|=1} \eta_{\mathbf{y}}\right] \right\rangle_{\Lambda, N}^{(T, E)}, \end{aligned} \quad (\text{B.16})$$

where we substituted the Hamiltonian (B.4). Here \mathbf{x} is one of $(j, 0)$, but it can actually be an arbitrary site in Λ because of the translation invariance.

Similarly we have

$$\tilde{c}(N_1 \rightarrow N_1 + 1) = \varepsilon \ell \left(1 - \frac{N_1}{V}\right) g(N_2) e^{\beta u_2}, \quad (\text{B.17})$$

for a hop from Λ_2 to Λ_1 .

B.3.2. Chemical Potential of Lattice Gases

To find the chemical potential let \tilde{N}_1 and \tilde{N}_2 be the average particle numbers in the steady state of the whole system. Since hops between the two sublattices balance with each other, we can assume that

$$\tilde{c}(\tilde{N}_1 \rightarrow \tilde{N}_1 - 1) = \tilde{c}(\tilde{N}_1 - 1 \rightarrow \tilde{N}_1). \quad (\text{B.18})$$

Then by using (B.15) and (B.17), we get

$$\frac{1}{\beta} \log \frac{g(\tilde{N}_1)}{1 - (\tilde{N}_1 - 1)/V} + u_1 = \frac{1}{\beta} \log \frac{g(\tilde{N}_2 + 1)}{1 - \tilde{N}_2/V} + u_2. \quad (\text{B.19})$$

By comparing this equality with our definition (5.3) of the chemical potential, we are led to define

$$\mu(\rho) = \frac{1}{\beta} \log \frac{g(\rho \ell h)}{1 - \rho + V^{-1}} \simeq \frac{1}{\beta} \log \frac{g(\rho \ell h)}{1 - \rho}, \quad (\text{B.20})$$

where $\rho = N/(\ell h)$ is the density. We assume that $\mu(\rho)$ defined by (B.20) has a sensible infinite volume limit $\ell, h \rightarrow \infty$ (i.e., $V \rightarrow \infty$). Then (B.19) precisely coincides with the desired balance Eq. (5.3).

Recalling the definitions (B.16) of $g(N)$, we stress that we have obtained a concrete formula (B.20) for the chemical potential which involve expectation values in the steady state. Therefore one can in principle compute $\mu(\rho) = \mu(T, E; V, N)$ by using systematic approximations or a computer. See

Sec. B.8. Note that our formula (B.20) for the chemical potential involves correlation functions of only local quantities. Therefore it is not affected by the long range power law correlations which are found universally in nonequilibrium steady states of lattice gases. This can be clearly seen in our perturbative calculation in Sec. B.8. See Sec. 8.3.2 for more discussions about long range correlations.

Note also that in (B.20) we have written down $\mu(\rho)$ without any ambiguities. To be precise, the relation (5.3) only determines the ρ dependence of the chemical potential. So there is a freedom to add any function $\mu_0(T, E)$ to (B.20). But the simplicity of the formula (B.20) suggests that this is the “right” choice. Indeed a consideration about μ -walls in Sec. B.7 indicates that (B.20) is the complete formula for the chemical potential.

B.3.3. Pressure of Lattice Gases

We shall define pressure for the driven lattice gas. Since lattice gas models do not have the notion of momentum, the standard definition in terms of mechanical forces do not apply. Instead we here obtain pressure from the mechanical work required to change the volume (area).

We consider two lattices with the same width ℓ and different heights h and \tilde{h} . We assume $h \gg \tilde{h}$. We place the smaller lattice on top of the larger one, and put them into a weak contact with each other as in Fig. 23. We apply a uniform potential u only to the smaller subsystem, and keep T and E constant over the whole system.

We first set $u = 0$ and let the whole system reach its steady state. Since the conditions are the same everywhere, we get a uniform local steady state with density ρ over the whole system. Then we slowly vary u from 0 to ∞ . When $u = \infty$, there are no particles in the smaller subsystem, and we have a uniform local steady state with T, E and the density $\rho\{1 + (\tilde{h}/h)\} \simeq \rho$ in the larger subsystem.

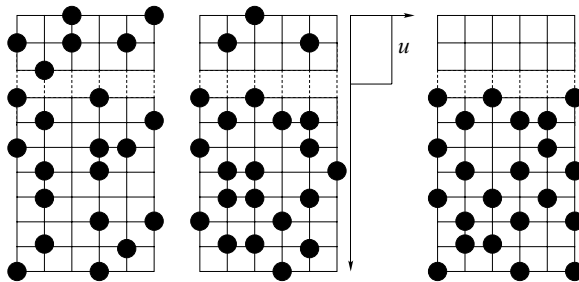


Fig. 23. The setting used to determine the pressure in the lattice gas. By changing the potential u applied to the smaller subsystem from 0 to ∞ , we can effectively reduce the volume (area) of the system by $\ell\tilde{h}$. From the mechanical work required to perform this change, we define the pressure.

Let $\tilde{\rho}(u)$ be the density in the smaller subsystem when the potential is u . By the balance condition (5.3), this density can be determined by

$$\mu(\rho) = \mu(\tilde{\rho}(u)) + u, \quad (\text{B.21})$$

where we set the density in the larger subsystem to ρ . This is allowed since the deviation is of order $\rho\tilde{h}/h$, and we can make \tilde{h}/h as small as we want. By differentiating (B.21) by u , we get

$$\frac{d\tilde{\rho}(u)}{du} = -\frac{1}{\mu'(\tilde{\rho}(u))}. \quad (\text{B.22})$$

Now we evaluate the mechanical work required to change the potential u . Since the total number of particles in the smaller subsystem is $\tilde{\rho}(u)\ell\tilde{h}$, the work needed to change the potential from u to $u + \Delta u$ is equal to $\Delta W = \Delta u \tilde{\rho}(u)\ell\tilde{h} + O((\Delta u)^2)$. The total work is obtained by summing this up as

$$W = \ell\tilde{h} \int_0^\infty du \tilde{\rho}(u) = \ell\tilde{h} \int_0^\rho d\tilde{\rho} \tilde{\rho} \mu'(\tilde{\rho}), \quad (\text{B.23})$$

where we used (B.22) to change the variable.

Defining the pressure p by the standard relation $W = p \Delta V$ with $\Delta V = \ell\tilde{h}$ being the volume (area) of the smaller subsystem, (B.23) implies

$$p(\rho) = \int_0^\rho d\tilde{\rho} \tilde{\rho} \mu'(\tilde{\rho}), \quad (\text{B.24})$$

which is the final formula of pressure in the lattice gas. Note that the Maxwell relation (5.4) is obvious from the formula (B.24).

B.3.4. Free Energy of Lattice Gases

Now that we have the formulae for the chemical potential (B.20) and the pressure (B.24), we use the Euler equation (6.2) in the form

$$f(\rho) = -p(\rho) + \rho \mu(\rho) = \int_0^\rho d\tilde{\rho} \mu(\tilde{\rho}), \quad (\text{B.25})$$

to define the specific free energy $f(\rho) = F(T, E; 1, \rho) = F(T, E; V, N)/V$ with $\rho = N/V$. The second equality in (B.25) is obtained by using the formula (B.24) and integrating by parts.

We have thus obtained concrete formulae for the chemical potential, the pressure, and the free energy of a nonequilibrium steady state of the lattice gas. The formulae only involve local correlation functions in the steady state distribution, and may be computed in a concrete model.

B.4. Steady State and Density Fluctuation

We will now study the steady state distribution of a weakly coupled system and show that Einstein’s formula (6.9) for the density fluctuation holds exactly in the present setting. Recall that in equilibrium statistical mechanics, the relation (6.9) follows trivially from the canonical distribution (Sec. 2.2). We note that an analogous derivation is never possible here since we still do not know anything about general forms of steady state distribution in nonequilibrium systems. Nevertheless the same relation can be proved by examining the effective stochastic process of particle exchange between the two subsystems.

Consider again the situation in Sec. B.3.1, where two identical systems on Λ_1 and Λ_2 are weakly coupled with each other. There are uniform potentials u_1 and u_2 on Λ_1 and Λ_2 , respectively.

We are interested in the steady state with the total particle number $|\eta| + |\zeta| = 2N$. When $\varepsilon = 0$, the distribution $p_{\Lambda_1, N_1}^{(T, E)}(\eta) p_{\Lambda_2, N_2}^{(T, E)}(\zeta)$ with any fixed N_1, N_2 such that $N_1 + N_2 = 2N$ is stationary.⁶¹ If we take into account the effect of $\varepsilon > 0$ in the lowest order, the above degeneracy is lifted and we get a unique steady state distribution of the form

$$p_{\Lambda_1, \Lambda_2; 2N}^{(T, E; u_1, u_2)}(\eta, \zeta) = \tilde{p}_{\Lambda_1, \Lambda_2; 2N}^{(T, E; u_1, u_2)}(|\eta|, |\zeta|) p_{\Lambda_1, |\eta|}^{(T, E)}(\eta) p_{\Lambda_2, |\zeta|}^{(T, E)}(\zeta), \tag{B.26}$$

where $\tilde{p}_{\Lambda_1, \Lambda_2; 2N}^{(T, E; u_1, u_2)}(N_1, N_2)$ is nonvanishing only when $N_1 + N_2 = 2N$. We again specify only N_1 , and abbreviate $\tilde{p}_{\Lambda_1, \Lambda_2; 2N}^{(T, E; u_1, u_2)}(N_1, N_2)$ simply as $\tilde{p}(N_1)$. It is the probability of finding N_1 particles in Λ_1 and $2N - N_1$ particles in Λ_2 , and is normalized as

$$\sum_{N_1} \tilde{p}(N_1) = 1. \tag{B.27}$$

We will now evaluate $\tilde{p}(N_1)$.

We substitute the steady state distribution (B.26) into the general condition (2.24) of stationarity, and then take partial sums over η and ζ with fixed $|\eta|$ and $|\zeta|$. By recalling the definition (B.14) of the effective transition rate for hop between the two sublattices, this gives

$$\sum_{\sigma=\pm 1} \{-\tilde{c}(N_1 \rightarrow N_1 + \sigma) \tilde{p}(N_1) + \tilde{c}(N_1 + \sigma \rightarrow N_1) \tilde{p}(N_1 + \sigma)\} = 0, \tag{B.28}$$

for any N_1 .

To solve (B.28), we try the ansatz

$$\tilde{p}(N_1) = q^{(u_1)}(N_1) q^{(u_2)}(2N - N_1), \tag{B.29}$$

⁶¹ Recall that $p_{\Lambda, N}^{(T, E)}(\eta)$ is the steady state distribution for the system on Λ , and is nonvanishing only when $|\eta| = N$.

with a function $q^{(u)}(N)$. We also assume that each term in the sum in the left-hand side of (B.28) vanishes. This is a kind of detailed balance condition. By using (B.15) and (B.17), we find that this condition is satisfied if

$$e^{\beta u} g(N) q^{(u)}(N) = \left(1 - \frac{N-1}{V}\right) q^{(u)}(N-1), \quad (\text{B.30})$$

which means

$$\begin{aligned} q^{(u)}(N) &= q^{(u)}(0) e^{-\beta u N} \prod_{M=1}^N \frac{1 - (M-1)/V}{g(M)} \\ &= \text{const.} \exp \left[-\beta u N - \beta \sum_{M=1}^N \mu \left(\frac{M}{V} \right) \right], \end{aligned} \quad (\text{B.31})$$

where we used (B.20). Note that

$$\sum_{M=1}^N \mu \left(\frac{M}{V} \right) \simeq V \int_0^\rho d\tilde{\rho} \mu(\tilde{\rho}) = V f(\rho), \quad (\text{B.32})$$

where we used (B.25) and wrote $\rho = N/V$. Thus from (B.31) and (B.29), we get the desired estimate

$$\tilde{p}_{\Lambda_1, \Lambda_2; 2N}^{(T, E; u_1, u_2)}(N_1, N_2) = \text{const.} \exp[-\beta V \{u_1 \rho_1 + u_2 \rho_2 + f(\rho_1) + f(\rho_2)\}], \quad (\text{B.33})$$

where $\rho_1 = N_1/V_1$ and $\rho_2 = N_2/V_2$.

If one sets $u_1 = u_2 = 0$, (B.33) becomes

$$\tilde{p}_{\Lambda_1, \Lambda_2; 2N}^{(T, E)}(N_1, N_2) = \text{const.} \exp[-\beta \{F(T, E; V, N_1) + F(T, E; V, N_2)\}], \quad (\text{B.34})$$

which is precisely Einstein's formula (6.9) for density fluctuation. It should be stressed that this is an exact relation, which covers both small fluctuations and large deviations. At least in the setting of weakly coupled lattice gases, we have shown rigorously that the density fluctuation in nonequilibrium steady states is exactly governed by the SST free energy.

It is easy to extend the fluctuation formula to the case where more than two subsystems are weakly coupled with each other.

B.5. Minimum Work Principle

Let us continue and study the steady state distribution in more detail. This will lead us to the minimum work principle for steady states.

By substituting (B.33) to the full expression (B.26) of the steady state distribution, we get the final formula for the steady state distribution

$$P_{\Lambda_1, \Lambda_2; 2N}^{(T, E; u_1, u_2)}(\boldsymbol{\eta}, \boldsymbol{\xi}) = c_0 e^{\beta \Phi(u_1, u_2) - \beta \{u_1 |\boldsymbol{\eta}| + u_2 |\boldsymbol{\xi}| + F(|\boldsymbol{\eta}|) + F(|\boldsymbol{\xi}|)\}} P_{\Lambda_1, |\boldsymbol{\eta}|}^{(T, E)}(\boldsymbol{\eta}) P_{\Lambda_2, |\boldsymbol{\xi}|}^{(T, E)}(\boldsymbol{\xi}), \tag{B.35}$$

for $\boldsymbol{\eta}$ and $\boldsymbol{\xi}$ such that $|\boldsymbol{\eta}| + |\boldsymbol{\xi}| = 2N$, where $F(N)$ is a shorthand for $F(T, E; V, N)$. We wrote the (unknown) normalization factor as⁶² $c_0 \exp[\beta \Phi(u_1, u_2)]$, where c_0 does not depend on u_1 and u_2 . We now investigate the function $\Phi(u_1, u_2)$, and show that it is nothing but a Legendre transformation of the free energy $F(N)$.

We fix all the parameters except u_1, u_2 , and denote the average over the distribution (B.35) as $\langle \dots \rangle_{u_1, u_2}$. Let us write

$$N_1(u_1, u_2) = \langle |\boldsymbol{\eta}| \rangle_{u_1, u_2}, \quad N_2(u_1, u_2) = \langle |\boldsymbol{\xi}| \rangle_{u_1, u_2}. \tag{B.36}$$

From the normalization condition

$$\sum_{\substack{\boldsymbol{\eta}, \boldsymbol{\xi} \\ (|\boldsymbol{\eta}| + |\boldsymbol{\xi}| = 2N)}} P_{\Lambda_1, \Lambda_2; 2N}^{(T, E; u_1, u_2)}(\boldsymbol{\eta}, \boldsymbol{\xi}) = 1, \tag{B.37}$$

and the expression (B.35), we find

$$\Phi(u_1, u_2) = -\frac{1}{\beta} \log \langle e^{-\beta(u_1 |\boldsymbol{\eta}| + u_2 |\boldsymbol{\xi}|)} \rangle_{0,0}. \tag{B.38}$$

By differentiating (B.38), we get

$$\frac{\partial \Phi(u_1, u_2)}{\partial u_1} = N_1(u_1, u_2), \quad \frac{\partial \Phi(u_1, u_2)}{\partial u_2} = N_2(u_1, u_2), \tag{B.39}$$

which can be regarded as differential equations for determining $\Phi(u_1, u_2)$.

We now claim that the solution of (B.39) is given by

$$\Phi(u_1, u_2) = \sum_{i=1}^2 \{F(N_i(u_1, u_2)) + u_i N_i(u_1, u_2)\}. \tag{B.40}$$

To see this, we simply differentiate (B.40) by u_1 to get

$$\frac{\partial \Phi(u_1, u_2)}{\partial u_1} = N_1(u_1, u_2) + \sum_{i=1}^2 \left[\frac{\partial N_i(u_1, u_2)}{\partial u_1} \left\{ \mu \left(\frac{N_i(u_1, u_2)}{V} \right) + u_i \right\} \right], \tag{B.41}$$

⁶² We may set $c_0 = 1$. But with the freedom of adjusting c_0 , we do not have to worry about additive constant in $\Phi(u_1, u_2)$.

where we used (6.4). Note that the balance condition (5.3) implies that $\mu(N_i(u_1, u_2)/V) + u_i$ is independent of $i = 1, 2$. Then since $N_1(u_1, u_2) + N_2(u_1, u_2) = 2N$ is constant, the second term in the right-hand side of (B.41) vanishes. We thus get the first equation in (B.39). The second equation follows similarly.

We have thus determined the steady state distribution (B.35) including the normalization function. The formula (B.40) shows that $\Phi(u_1, u_2)$ is obtained from $F(T, E; V, N)$ by a Legendre transformation.

At this stage we shall see what we get from the general second law of Markov processes described in Appendix C.

We consider a time-dependent Markov process where the potentials $u_1(t)$, $u_2(t)$ become time-dependent in the present model. The pair (u_1, u_2) correspond to the parameter α in Appendix C. The system is initially in the steady state corresponding to $(u_1(0), u_2(0))$, and we vary $u_1(t)$, $u_2(t)$ in an arbitrary manner for $0 \leq t \leq t_f$.

Using (B.35), we see that the function $\varphi^{(\alpha)}$ of (C.2), which plays a fundamental role in the second law, becomes

$$\varphi^{(u_1, u_2)}(\boldsymbol{\eta}, \boldsymbol{\zeta}) = \beta\{u_1|\boldsymbol{\eta}| + u_2|\boldsymbol{\zeta}| - \Phi(u_1, u_2)\} - \log p_{\Lambda_1, \Lambda_2; 2N}^{(T, E; 0, 0)}(\boldsymbol{\eta}, \boldsymbol{\zeta}). \quad (\text{B.42})$$

Therefore the second law reads

$$\int_0^{t_f} dt \left\{ \frac{du_1(t)}{dt} \langle |\boldsymbol{\eta}| \rangle_t + \frac{du_2(t)}{dt} \langle |\boldsymbol{\zeta}| \rangle_t \right\} \geq \Phi(u_1(t_f), u_2(t_f)) - \Phi(u_1(0), u_2(0)). \quad (\text{B.43})$$

Since $\langle |\boldsymbol{\eta}| \rangle_t$ and $\langle |\boldsymbol{\zeta}| \rangle_t$ are the number of particles in Λ_1 and Λ_2 , respectively, the left-hand side of (B.43) is precisely the mechanical work W needed to change the potentials $u_1(t)$, $u_2(t)$. Thus (B.43) becomes

$$W \geq \Phi(u_1(t_f), u_2(t_f)) - \Phi(u_1(0), u_2(0)), \quad (\text{B.44})$$

which is the minimum work principle for steady states. Note that Φ rather than F appears on the right-hand side because we are controlling the potentials u_1 , u_2 , rather than the volume. If we set $u_1(0) = u_2(0) = 0$ and $u_1(t_f) = 0$, $u_2(t_f) = \infty$, then (B.44) becomes

$$\begin{aligned} W &\geq F(T, E; V, 2N) - 2F(T, E; V, N) \\ &= F(T, E; V, 2N) - F(T, E; 2V, 2N), \end{aligned} \quad (\text{B.45})$$

which is precisely of the form (6.11) of the conjectured minimum work principle.

It is an easy exercise to extend the minimum work principle (B.44) to the cases where n subsystems are weakly coupled with each other. Then one is allowed to change the potentials $u_1(t), \dots, u_n(t)$ in an arbitrary manner.

The present minimum work principle, although valid for any $u_1(t)$, $u_2(t)$, may not be too exciting since weak coupling ensures that each subsystem is in a steady state for any t . But see the following remark.

Remark: The essences of the minimum work principle (B.44) may be the following property that we shall call “weak canonicity.” Consider a Markov process for a lattice gas, and let $p_0(\boldsymbol{\eta})$ be the stationary distribution for the case where no potential is applied to the system. We then apply a potential $u(\cdot)$ to the system and denote the new stationary distribution as $p_{u(\cdot)}(\boldsymbol{\eta})$.

We say that the system has “weak canonicity” for a class of potentials \mathcal{U} if

$$p_{u(\cdot)}(\boldsymbol{\eta}) \simeq \exp \left[\beta \Phi[u(\cdot)] - \beta \sum_{x \in \Lambda} u(x) \eta_x \right] p_0(\boldsymbol{\eta}), \quad (\text{B.46})$$

for any $u(\cdot) \in \mathcal{U}$, where the function $\Phi[u(\cdot)]$ ensures the normalization.

If (B.46) holds we can easily show a minimum work principle

$$W \geq \Phi[u_t(\cdot)] - \Phi[u_0(\cdot)], \quad (\text{B.47})$$

for a time-dependent Markov process where $u_t(\cdot)$ varies within \mathcal{U} . We can also show the expected formula for density fluctuation and a version of fluctuation-response relation based on (B.46).

We therefore regard it an important task to study which models possess weak canonicity for which classes of potentials. So far we only know of some simple examples.

B.6. Linear Response

We can also develop a linear response theory for time-dependent phenomena which take place when the potentials u_1 , u_2 become time-dependent. As we have already remarked in Sec. A.4, it may not be too surprising that we can study linear transport phenomena, since we are dealing only with transport through the weak contact. Nevertheless it might be of some importance that a linear response theory in a highly nonequilibrium system can be constructed unambiguously. Recent numerical study⁽⁸⁴⁾ indicates the validity of the fluctuation response relation in DLG when a weak probing field orthogonal to the strong driving field is applied. This finding is similar to the result we present here, but (theoretically speaking) is more delicate.

Since the potential affects only hopping between Λ_1 and Λ_2 , we only need to treat slow stochastic dynamics of particle exchange. We again fix the total number of particles to $2N$, and only specify N_1 , the number of particles in Λ_1 .

For simplicity⁶³ we set $u_1 = 0$ and $u_2 = \lambda h(t)$, where $h(t)$ is an arbitrary (not too pathological) function such that $h(t) = 0$ for $t < 0$. λ is a small parameter in which we shall expand. We denote by $\tilde{p}_t(N_1)$ the probability that there are N_1 particles in Λ_1 (and hence $2N - N_1$ particles in Λ_2) at time t . It satisfies the master equation

$$\begin{aligned} \frac{d}{dt} \tilde{p}_t(N_1) &= \sum_{\sigma=\pm 1} \{-\tilde{p}_t(N_1) \tilde{c}_\lambda(N_1 \rightarrow N_1 + \sigma) \\ &\quad + \tilde{p}_t(N_1 + \sigma) \tilde{c}_\lambda(N_1 + \sigma \rightarrow N_1)\}, \end{aligned} \quad (\text{B.48})$$

for any $t \geq 0$ and N_1 , where $\tilde{c}_\lambda(N_1 \rightarrow N_1 + \sigma)$ is the transition rate (B.15) or (B.17) with $u_1 = 0$ and $u_2 = \lambda h(t)$. The initial distribution $\tilde{p}_0(N_1)$ is taken to be the stationary distribution (studied in Sec. B.4) with $u_1 = u_2 = 0$. We wish to solve (B.48) in the lowest order of λ .

From (B.15) and (B.17), we find that

$$\tilde{c}_\lambda(N_1 \rightarrow N_1 - 1) = \tilde{c}_0(N_1 \rightarrow N_1 - 1) \quad (\text{B.49})$$

and

$$\begin{aligned} \tilde{c}_\lambda(N_1 \rightarrow N_1 + 1) &= \tilde{c}_0(N_1 \rightarrow N_1 + 1) e^{\lambda \beta h(t)} \\ &= \tilde{c}_0(N_1 \rightarrow N_1 + 1) \\ &\quad + \lambda \beta h(t) \tilde{c}_0(N_1 \rightarrow N_1 + 1) + O(\lambda^2). \end{aligned} \quad (\text{B.50})$$

By substituting (B.49) and (B.50) into the master equation (B.48), we get

$$\begin{aligned} \frac{d}{dt} \tilde{p}_t(N_1) &= \sum_{N'_1} \Gamma(N_1, N'_1) \tilde{p}_t(N'_1) \\ &\quad + \lambda \beta h(t) \{-\tilde{p}_t(N_1) \tilde{c}_0(N_1 \rightarrow N_1 + 1) + \tilde{p}_t(N_1 - 1) \\ &\quad \times \tilde{c}_0(N_1 - 1 \rightarrow N_1)\} + O(\lambda^2), \end{aligned} \quad (\text{B.51})$$

where we have defined $\Gamma(N_1, N'_1)$ by

$$\begin{aligned} \sum_{N'_1} \Gamma(N_1, N'_1) q(N'_1) &= \sum_{\sigma=\pm 1} \{-q(N_1) \tilde{c}_0(N_1 \rightarrow N_1 + \sigma) \\ &\quad + q(N_1 + \sigma) \tilde{c}_0(N_1 + \sigma \rightarrow N_1)\}, \end{aligned} \quad (\text{B.52})$$

for any $q(\cdot)$.

⁶³ Extension to models with varying u_1 is automatic.

The time evolution operator $U_t(N_1, N'_1)$ for $u_1 = u_2 = 0$ is defined as the solution of

$$\frac{d}{dt}U_t(N_1, N'_1) = \sum_{N''_1} \Gamma(N_1, N''_1) U_t(N''_1, N'_1), \quad (\text{B.53})$$

with the initial condition $U_0(N_1, N'_1) = \delta_{N_1, N'_1}$. Then it is standard⁶⁴ that the perturbative solution of the master equation (B.51) is given by

$$\begin{aligned} \tilde{p}_t(N_1) &= \tilde{p}_0(N_1) + \lambda \beta \int_0^t ds \sum_{N'_1} U_{t-s}(N_1, N'_1) h(s) \\ &\quad \times \{-\tilde{p}_0(N'_1) \tilde{c}_0(N'_1 \rightarrow N'_1 + 1) + \tilde{p}_0(N'_1 - 1) \tilde{c}_0(N'_1 - 1 \rightarrow N'_1)\} \\ &\quad + O(\lambda^2) \\ &= \tilde{p}_0(N_1) - \lambda \beta \int_0^t ds \sum_{N'_1} \sum_{\sigma=\pm 1} U_{t-s}(N_1, N'_1) h(s) \sigma \tilde{p}_0(N'_1 + \sigma) \\ &\quad \times \tilde{c}_0(N'_1 + \sigma \rightarrow N'_1) + O(\lambda^2), \end{aligned} \quad (\text{B.54})$$

where we used the detailed balance condition $\tilde{p}_0(N'_1) \tilde{c}_0(N'_1 \rightarrow N'_1 + 1) = \tilde{p}_0(N'_1 + 1) \tilde{c}_0(N'_1 + 1 \rightarrow N'_1)$ to get the final expression.

We define the “current operator” by

$$j_{N_1, N'_1} = \tilde{c}_0(N'_1 \rightarrow N_1) (N'_1 - N_1), \quad (\text{B.55})$$

which measures the number of particle (which number is either 0, 1 or -1) that have passed from Λ_1 to Λ_2 at a given instant. Then the solution (B.54) can be written in the form

$$\tilde{p}_t(N_1) = \tilde{p}_0(N_1) - \lambda \beta \int_0^t ds \sum_{N'_1, N''_1} U_{t-s}(N_1, N'_1) h(s) j_{N'_1, N''_1} \tilde{p}_0(N''_1) + O(\lambda^2), \quad (\text{B.56})$$

which is the basic equation of our linear response theory.

The average $\langle \hat{N}_1(t) \rangle_\lambda = \sum_{N_1} N_1 \tilde{p}_t(N_1)$ of the number of particles in Λ_1 at time t can be evaluated by using (B.56) as

$$\langle \hat{N}_1(t) \rangle_\lambda = N - \lambda \beta \int_0^t ds \sum_{N_1, N'_1, N''_1} N_1 U_{t-s}(N_1, N'_1) h(s) j_{N'_1, N''_1} \tilde{p}_0(N''_1) + O(\lambda^2), \quad (\text{B.57})$$

⁶⁴A quick derivation. Here we write N instead of N_1 . Write (B.51) as $d\tilde{p}_t(N)/dt = \sum_{N'} \{\Gamma(N, N') + \lambda \chi_t(N, N')\} \tilde{p}_t(N) + O(\lambda^2)$, and write the solution as $\tilde{p}_t(N) = \tilde{p}_0 + \lambda q_t(N) + O(\lambda^2)$. Then by noting that $\sum_{N'} \Gamma(N, N') \tilde{p}_0(N') = 0$, one finds that $q_t(N)$ satisfies the differential equation $dq_t(N)/dt = \sum_{N'} \Gamma(N, N') q_t(N') + \lambda \sum_{N'} \chi_t(N, N') \tilde{p}_0(N')$. It is easy to check that the solution is written as $q_t(N) = \int_0^t ds \sum_{N', N''} U_{t-s}(N, N') \chi_s(N', N'') p_0(N'')$.

where we noted that the average in the steady state with $u_1 = u_2 = 0$ satisfies $\sum_{N_1} N_1 \tilde{p}_0(N_1) = N$. We can further rewrite (B.57) as

$$\langle \hat{N}_1(t) \rangle_\lambda = N - \lambda \beta \int_0^t ds h(s) \langle \hat{N}_1(t) \hat{j}(s) \rangle_0 + O(\lambda^2), \quad (\text{B.58})$$

where the definition of the time-dependent correlation function $\langle \hat{N}_1(t) \hat{j}(s) \rangle_0$ may be clear by comparing (B.58) with (B.57). This is the desired fluctuation-response relation for the particle exchange process in the weakly coupled DLG.

When $h(t)$ is a step function with $h(t) = 0$ for $t < 0$ and $h(t) = 1$ for $t \geq 0$, then (B.58) simplifies as

$$\begin{aligned} \langle \hat{N}_1(t) \rangle_\lambda &= N - \lambda \beta \int_0^t ds \langle \hat{N}_1(t) \hat{j}(s) \rangle_0 + O(\lambda^2) \\ &= N + \lambda \beta \langle \hat{N}_1(t) \{ \hat{N}_1(t) - \hat{N}_1(0) \} \rangle_0 + O(\lambda^2). \end{aligned} \quad (\text{B.59})$$

B.7. μ -Wall in the Driven Lattice Gas

Let us comment on how the notion of μ -walls introduced in Sec. 7.1 can be implemented in the driven lattice gas.

The answer seems to be very simple. The weak coupling scheme of Sec. B.3.1 can be applied to situations where the subsystems on Λ_1 and Λ_2 have different values of nonequilibrium parameters. If we set $E = 0$ for the subsystem on Λ_2 , a contact between a steady state and an equilibrium state is realized. We may assume that this weak coupling realizes a μ -wall. (But see the remark at the end of this section.)

To see that this defines $\mu(T, E; V, N)$ consistently (see the discussion at the end of Sec. 7.1), it suffices to show that the formula (B.20) gives the standard chemical potential for equilibrium states. This fact can be checked directly for general cases, but the easiest way is to treat the free system with $H_\Lambda(\cdot) = 0$ at equilibrium. Then (B.20) gives

$$\mu(\rho) = \frac{1}{\beta} \log \frac{\rho}{1 - \rho}, \quad (\text{B.60})$$

which coincides with the result from equilibrium statistical mechanics. Since it is guaranteed that two systems in a weak contact have the same values of $\mu(\rho)$, it follows that (B.20) gives the equilibrium chemical potential in an arbitrary equilibrium system.

We therefore conclude that the formula (B.20) gives a consistent chemical potential $\mu(T, E; V, N)$ for a local steady state $(T, E; V, N)$ including its dependence on T and E . Similarly the formula (B.25) defines the corresponding free energy $F(T, E; V, N)$ without ambiguity.

It should be recalled, however, that we concluded in Sec. 7.1 that a contact between an equilibrium state and a nonequilibrium steady state cannot be realized in the $(T, \phi; V, N)$ formalism. If we stick onto the interpretation that E represents the electric field, we must again conclude that our contact is not realistic. Nevertheless the fact that we can construct (at least theoretically) a consistent μ -wall may be of importance and interest.

B.8. Perturbative Estimate of the SST Free Energy

We found that (B.20) can be regarded as the definition of SST chemical potential for the steady state in the driven lattice gas. It is worth trying to evaluate this and other thermodynamic quantities explicitly. Since exact calculations are so far impossible, we here calculate the leading contributions in the limit of low density and high temperature.

First by substituting the definition (B.16) of $g(N)$ into the chemical potential (B.20), and expanding the exponential, we get

$$\mu(\rho) = \frac{1}{\beta} \log \frac{\rho - \beta J \sum_{y:|y-x|=1} \langle \eta_x \eta_y \rangle + O(\rho^3)}{1 - \rho}, \quad (\text{B.61})$$

where we noted that $\langle \eta_x \rangle = \rho$. In the present section we consider a uniform system on Λ , and suppress the suffixes T, E, Λ , and N because they are always fixed. We thus need to evaluate the two-point correlation function $\langle \eta_x \eta_y \rangle$.

We evaluate the leading nonequilibrium correction to $\langle \eta_x \eta_y \rangle$ by using the standard procedure. One first notes that, for any function $h(\boldsymbol{\eta})$ of the configuration, there is an identity

$$\sum_{\boldsymbol{\eta}} p(\boldsymbol{\eta}) \sum_{\langle u,v \rangle} c(\boldsymbol{\eta} \rightarrow \boldsymbol{\eta}^{u,v}) \{h(\boldsymbol{\eta}^{u,v}) - h(\boldsymbol{\eta})\} = 0, \quad (\text{B.62})$$

which follows from the master equation (2.23). $p(\boldsymbol{\eta})$ is the steady state distribution. We here set $h(\boldsymbol{\eta}) = \eta_x \eta_y$. We substitute the transition rate (B.6) into (B.62) and keep only those terms which have order ρ^2 . After a straightforward (but a little tedious) calculation, we get

$$\begin{aligned} & \sum_{\substack{\mathbf{u} \in \Lambda \\ |\mathbf{u}-\mathbf{x}|=1, \mathbf{u} \neq \mathbf{y}}} \left\{ -\phi(\beta\{J_{x,y} - J_{u,y} + E(x_1 - u_1)\}) \tilde{G}(\mathbf{x}, \mathbf{y}) \right. \\ & \quad \left. + \phi(\beta\{J_{u,y} - J_{x,y} + E(u_1 - x_1)\}) \tilde{G}(\mathbf{u}, \mathbf{y}) \right\} \\ & + \sum_{\substack{\mathbf{v} \in \Lambda \\ |\mathbf{v}-\mathbf{x}|=1, \mathbf{v} \neq \mathbf{x}}} \left\{ -\phi(\beta\{J_{x,y} - J_{x,v} + E(y_1 - v_1)\}) \tilde{G}(\mathbf{x}, \mathbf{y}) \right. \\ & \quad \left. + \phi(\beta\{J_{x,v} - J_{x,y} + E(v_1 - y_1)\}) \tilde{G}(\mathbf{x}, \mathbf{v}) \right\} = O(\rho^3), \quad (\text{B.63}) \end{aligned}$$

where $\tilde{G}(\mathbf{x}, \mathbf{y}) = \langle \eta_{\mathbf{x}} \eta_{\mathbf{y}} \rangle$, and $J_{\mathbf{x}, \mathbf{y}} = J$ if $|\mathbf{x} - \mathbf{y}| = 1$ and $J_{\mathbf{x}, \mathbf{y}} = 0$ otherwise. Since $\sum_{\mathbf{x}} \eta_{\mathbf{x}} = N$, the two point function $\tilde{G}(\mathbf{x}, \mathbf{y})$ must satisfy $\sum_{\mathbf{x}, \mathbf{y}} \tilde{G}(\mathbf{x}, \mathbf{y}) = N(N - 1)$. This normalization condition and the Eq. (B.63) determines $\tilde{G}(\mathbf{x}, \mathbf{y})$ (to the order ρ^2).

By using the translation invariance, we can write $\tilde{G}(\mathbf{x}, \mathbf{y}) = G(\mathbf{x} - \mathbf{y}) + O(\rho^3)$ with a function $G(\mathbf{x})$ of $\mathbf{x} \in \Lambda \setminus \{\mathbf{o}\}$. Here $\mathbf{o} = (0, 0)$ is the origin. From (B.63), we see that $G(\mathbf{x})$ satisfies the equation⁶⁵

$$\sum_{\substack{\mathbf{y} \in \Lambda \\ |\mathbf{x} - \mathbf{y}| = 1, \mathbf{y} \neq \mathbf{o}}} \{-\tilde{c}(\mathbf{x} \rightarrow \mathbf{y}) G(\mathbf{x}) + \tilde{c}(\mathbf{y} \rightarrow \mathbf{x}) G(\mathbf{y})\} = 0, \quad (\text{B.64})$$

for any $\mathbf{x} \in \Lambda$. Here the effective transition rate is given by

$$\tilde{c}(\mathbf{x} \rightarrow \mathbf{y}) = \phi(\beta\{J_{\mathbf{x}} - J_{\mathbf{y}} + E(x_1 - y_1)\}) + \phi(\beta\{J_{\mathbf{x}} - J_{\mathbf{y}} + E(y_1 - x_1)\}), \quad (\text{B.65})$$

with $J_{\mathbf{x}} = J$ if $|\mathbf{x}| = 1$ and $J_{\mathbf{x}} = 0$ otherwise.

Let us denote the unit vectors as $\mathbf{e}_1 = (1, 0)$ and $\mathbf{e}_2 = (0, 1)$. We introduce $\mathcal{U} = \{\mathbf{e}_1, -\mathbf{e}_1, \mathbf{e}_2, -\mathbf{e}_2\}$, which is the set of sites neighboring to the origin \mathbf{o} . Now unless \mathbf{x} or \mathbf{y} is in \mathcal{U} , we have $\tilde{c}(\mathbf{x} \rightarrow \mathbf{y}) = t \equiv \phi(\beta E) + \phi(-\beta E)$ if $\mathbf{x} - \mathbf{y} = \pm \mathbf{e}_1$, and $\tilde{c}(\mathbf{x} \rightarrow \mathbf{y}) = s \equiv 2\phi(0)$ if $\mathbf{x} - \mathbf{y} = \pm \mathbf{e}_2$. The effective hopping rate $\tilde{c}(\mathbf{x} \rightarrow \mathbf{y})$ become irregular only around the origin. More precisely, for $\mathbf{x} \in \mathcal{U}$, we have $\tilde{c}(\mathbf{x} \rightarrow \mathbf{x} \pm \mathbf{e}_1) = \phi(\beta\{J + E\}) + \phi(\beta\{J - E\})$, $\tilde{c}(\mathbf{x} \pm \mathbf{e}_1 \rightarrow \mathbf{x}) = \phi(-\beta\{J + E\}) + \phi(-\beta\{J - E\})$, $\tilde{c}(\mathbf{x} \rightarrow \mathbf{x} \pm \mathbf{e}_2) = 2\phi(\beta J)$, and $\tilde{c}(\mathbf{x} \pm \mathbf{e}_2 \rightarrow \mathbf{x}) = 2\phi(-\beta J)$.

By explicitly separating the equilibrium behavior in $G(\mathbf{x})$, we write

$$G(\mathbf{x}) = G_0 e^{\beta J_{\mathbf{x}}} (1 + \psi_{\mathbf{x}}), \quad (\text{B.66})$$

where $\psi_{\mathbf{x}}$ is the nonequilibrium correction which vanishes if $E = 0$, and G_0 is the normalization constant. By substituting (B.66) into (B.64), we get

$$\sum_{\substack{\mathbf{y} \in \Lambda \\ |\mathbf{x} - \mathbf{y}| = 1, \mathbf{y} \neq \mathbf{o}}} \{-t(\mathbf{x} \rightarrow \mathbf{y})(1 + \psi_{\mathbf{x}}) + t(\mathbf{y} \rightarrow \mathbf{x})(1 + \psi_{\mathbf{y}})\} = 0, \quad (\text{B.67})$$

where the hopping rates are written as

$$t(\mathbf{x} \rightarrow \mathbf{y}) = t^{(0)}(\mathbf{x} \rightarrow \mathbf{y}) + \Delta t(\mathbf{x} \rightarrow \mathbf{y}), \quad (\text{B.68})$$

with $t^{(0)}(\mathbf{x} \rightarrow \mathbf{x} \pm \mathbf{e}_1) = t$ and $t^{(0)}(\mathbf{x} \rightarrow \mathbf{x} \pm \mathbf{e}_2) = s$ for any $\mathbf{x} \in \Lambda$. As for the correction near the origin, we have, for $\mathbf{x} \in \mathcal{U}$,

$$\Delta t(\mathbf{x} \rightarrow \mathbf{x} \pm \mathbf{e}_1) = e^{\beta J} \{\phi(\beta\{J + E\}) + \phi(\beta\{J - E\})\} - \{\phi(\beta E) + \phi(-\beta E)\},$$

$$\Delta t(\mathbf{x} \pm \mathbf{e}_1 \rightarrow \mathbf{x}) = \phi(-\beta\{J + E\}) + \phi(-\beta\{J - E\}) - \{\phi(\beta E) + \phi(-\beta E)\},$$

⁶⁵ This is the same equation as one gets for the driven lattice gas with only two particles as studied in Ref. 81.

$$\begin{aligned} \Delta t(\mathbf{x} \rightarrow \mathbf{x} \pm \mathbf{e}_2) &= 2e^{\beta J} \phi(\beta J) - 2\phi(0), \\ \Delta t(\mathbf{x} \pm \mathbf{e}_2 \rightarrow \mathbf{x}) &= 2\phi(-\beta J) - 2\phi(0), \end{aligned} \tag{B.69}$$

and $\Delta t(\mathbf{x} \rightarrow \mathbf{y}) = 0$ for other combinations.

Note that $\Delta t(\mathbf{x} \rightarrow \mathbf{y}) \rightarrow 0$ as $\beta \rightarrow 0$. We thus neglect the cross terms $\Delta t \psi$ in (B.67) to get the lowest order contribution for ψ_x in the limit of high temperature. The result is

$$\sum_{\substack{\mathbf{y} \in \Lambda \\ |\mathbf{x}-\mathbf{y}|=1, \mathbf{y} \neq \mathbf{o}}} \{ -t^{(0)}(\mathbf{x} \rightarrow \mathbf{y})\psi_x + t^{(0)}(\mathbf{y} \rightarrow \mathbf{x})\psi_y \} = -Q_x, \tag{B.70}$$

with

$$Q_x = \sum_{\substack{\mathbf{y} \in \Lambda \\ |\mathbf{x}-\mathbf{y}|=1, \mathbf{y} \neq \mathbf{o}}} \{ \Delta t(\mathbf{y} \rightarrow \mathbf{x}) - \Delta t(\mathbf{x} \rightarrow \mathbf{y}) \}. \tag{B.71}$$

Note that (B.70) is nothing but the Laplace-Poisson equation on the two-dimensional lattice with charge distribution Q_x .

The charge Q_x can be calculated using the explicit forms (B.69) of $\Delta t(\mathbf{x} \rightarrow \mathbf{y})$ and the (local detailed balance) condition $\phi(h) = e^{-h} \phi(-h)$, which is (2.28). After a little calculation one finds that $Q_{\pm \mathbf{e}_1} = Q_0$, $Q_{\pm 2\mathbf{e}_1} = -Q_0$, $Q_{\pm \mathbf{e}_2} = 2Q_0$, $Q_{\pm \mathbf{e}_1 \pm \mathbf{e}_2} = Q_{\pm \mathbf{e}_1 \mp \mathbf{e}_2} = -Q_0$, and $Q_x = 0$ otherwise, where

$$\begin{aligned} Q_0 &= \phi(-\beta\{J - E\}) + \phi(-\beta\{J + E\}) - e^{\beta J} \{ \phi(\beta\{J + E\}) + \phi(\beta\{J - E\}) \} \\ &= (1 - e^{\beta E})\phi(-\beta\{J - E\}) + (1 - e^{-\beta E})\phi(-\beta\{J + E\}). \end{aligned} \tag{B.72}$$

As can be seen from Fig. 24, the charge distribution Q_x is a collection of quadrupoles.

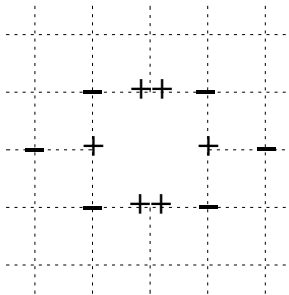


Fig. 24. The nonequilibrium correction ψ_x is the solution of the Laplace-Poisson equation with the charge distribution Q_x . The symbols +, - represents the charge Q_0 and $-Q_0$. Note that this is a collection of quadrupoles.

Clearly one has $Q_0 = 0$ if $E = 0$. By expanding in β , we find that the leading behavior of Q_0 is

$$Q_0 = \frac{\beta^3}{2} E^2 J(4\phi''(0) - \phi(0)), \quad (\text{B.73})$$

where we assumed that $\phi(h)$ is differentiable, and used the fact that (2.28) implies $\phi'(0) = -\phi(0)/2$.

Thus the nonequilibrium correction ψ_x can be obtained by solving the Laplace-Poisson equation (B.70) with the charge distribution Q_x of Fig. 24. Note also that, to get the lowest order behavior in β , we can set $t = s = 2\phi(0)$. Since the charge distribution is a collection of quadrupoles, the long range behavior of ψ_x is given by

$$\psi_x \approx \frac{(x_1)^2 - (x_2)^2}{|x|^4}, \quad (\text{B.74})$$

which is the famous $1/r^d$ long range correlation (see Refs. 20, 81, 92). But we are here interested only in the very short range behavior, i.e., the values of ψ_x for $x \in \mathcal{U}$. Clearly for $x \in \mathcal{U}$, the solution of (B.70) is given by $\psi_x \simeq \text{const. } Q_0/t$ with positive constants. It is not an easy task to determine the constants, but they are certainly numerical constants (which do not depend on any of the model parameters) of order 1.

We therefore conclude that the leading correction in the nearest neighbor correlation function is given as

$$\sum_{y:|y-x|=1} \langle \eta_x \eta_y \rangle \simeq \sum_{y:|y-x|=1} \langle \eta_x \eta_y \rangle^{\text{eq}} + C \left(4 \frac{\phi''(0)}{\phi(0)} - 1 \right) \beta^3 E^2 J \rho^2, \quad (\text{B.75})$$

where $\langle \dots \rangle^{\text{eq}}$ denotes the expectation in the corresponding equilibrium, and C is a positive numerical constant which does not depend on any of the model parameters (and may be computed numerically if necessary).

By substituting (B.75) into (B.61) and further expanding, we finally get

$$\mu(T, E; \rho) \simeq \mu(T, 0; \rho) - C \left(4 \frac{\phi''(0)}{\phi(0)} - 1 \right) \beta^3 E^2 J^2 \rho. \quad (\text{B.76})$$

By substituting this into (B.25), we get

$$f(T, E; \rho) \simeq f(T, 0; \rho) - \frac{C}{2} \left(4 \frac{\phi''(0)}{\phi(0)} - 1 \right) \beta^3 E^2 J^2 \rho^2, \quad (\text{B.77})$$

which is the concrete form of SST free energy for the driven lattice gas.

One of our postulates of SST stated in Sec. 7.3 is that the free energy $f(T, E; \rho)$ is a concave function of E , i.e., $\partial^2 f(T, E; \rho) / \partial E^2 \leq 0$. It is apparent from (B.77) that the validity of this postulate depends crucially on the choice of the function $\phi(h)$. As for the most standard heat-bath rule with $\phi(h) = (1 + e^h)^{-1}$,

we have $\phi''(0) = 0$, which means that $f(T, E; \rho)$ does not satisfy the conjectured concavity.

C. THE “SECOND LAW” FOR A GENERAL TIME-DEPENDENT MARKOV PROCESS

Let us state and prove the “second law” in a Markov process which was used in Secs. 2.3.3 and B.5.

C.1. Main Results

Let \mathcal{S} be a finite state space, and $c^{(\alpha)}(s \rightarrow s')$ be arbitrary transition rates which ensure ergodicity. (See Sec. 2.3.1 for the general setup.) By $p_\infty^{(\alpha)}(s)$ we denote the stationary distribution for the time-independent Markov process with constant transition rates $c^{(\alpha)}(s \rightarrow s')$. More precisely it satisfies

$$\sum_{\substack{s' \in \mathcal{S} \\ (s' \neq s)}} \{ -c^{(\alpha)}(s \rightarrow s') p_\infty^{(\alpha)}(s) + c^{(\alpha)}(s' \rightarrow s) p_\infty^{(\alpha)}(s') \} = 0, \quad (C.1)$$

for any $s \in \mathcal{S}$. (See (2.24).) Let us define

$$\varphi^{(\alpha)}(s) = -\log p_\infty^{(\alpha)}(s). \quad (C.2)$$

Fix an arbitrary differentiable function $\alpha(t)$ with $0 \leq t \leq t_f$, and consider a time-dependent Markov process with the transition rates $c^{(\alpha(t))}(s \rightarrow s')$. The probability distribution $p_t(s)$ at time t satisfies the master equation

$$\frac{d}{dt} p_t(s) = \sum_{\substack{s' \in \mathcal{S} \\ (s' \neq s)}} \{ -c^{(\alpha(t))}(s \rightarrow s') p_t(s) + c^{(\alpha(t))}(s' \rightarrow s) p_t(s') \}, \quad (C.3)$$

for any $s \in \mathcal{S}$. We set the initial condition as

$$p_0(s) = p_\infty^{(\alpha(0))}(s). \quad (C.4)$$

We denote the average over $p_t(s)$ as $\langle g(s) \rangle_t = \sum_{s \in \mathcal{S}} g(s) p_t(s)$.

Then the well known “second law” is

$$\int_0^{t_f} dt \frac{d\alpha(t)}{dt} \left\langle \frac{d}{d\alpha} \varphi^{(\alpha)}(s) \Big|_{\alpha=\alpha(t)} \right\rangle_t \geq 0. \quad (C.5)$$

C.2. Proof

For completeness we prove the “second law” (C.5). Although the standard proof makes use of relative entropy (see, for example, Sec. 2.9 of Ref. 93), we here present a direct proof.

Only in the present proof, we make use of the probabilistic language and denote by $\hat{s}(t)$ the random variables for the present Markov process. Thus $p_t(s) = \text{Prob}[\hat{s}(t) = s]$.

Fix a positive integer N , and let $\Delta t = t_f/N$. Let⁶⁶

$$T^t(s, s') = \text{Prob}[\hat{s}(t) = s \mid \hat{s}(t - \Delta t) = s']. \tag{C.6}$$

In physicists' language, $T^t(s, s')$ is the time-evolution kernel from $t - \Delta t$ to t , since it satisfies

$$p_t(s) = \sum_{s' \in \mathcal{S}} T^t(s, s') p_{t-\Delta t}(s'), \tag{C.7}$$

where $p_t(s)$ is the solution of the master Eq. (C.3) with an arbitrary initial condition. Note that

$$\sum_{s' \in \mathcal{S}} T^t(s, s') p_\infty^{(\alpha(t))}(s') = p_\infty^{(\alpha(t))}(s) + O((\Delta t)^2). \tag{C.8}$$

For $n = 0, 1, \dots, N$, let $t_n = n \Delta t$. Define a random quantity

$$\hat{Q} = \prod_{n=0}^{N-1} \frac{p_\infty^{(\alpha(t_{n+1}))}(\hat{s}(t_{n+1}))}{p_\infty^{(\alpha(t_n))}(\hat{s}(t_n))}. \tag{C.9}$$

By using (C.8) repeatedly, we find that

$$\begin{aligned} \langle \hat{Q} \rangle &= \sum_{s_0, s_1, \dots, s_{N-1} \in \mathcal{S}} \left\{ \prod_{n=1}^{N-1} T^{t_n}(s_n, s_{n-1}) \right\} p_\infty^{\alpha(t_0)}(s_0) \prod_{n=0}^{N-1} \frac{p_\infty^{(\alpha(t_{n+1}))}(s_n)}{p_\infty^{(\alpha(t_n))}(s_n)} \\ &= \sum_{s_1, \dots, s_{N-1} \in \mathcal{S}} \left\{ \prod_{n=2}^{N-1} T^{t_n}(s_n, s_{n-1}) \right\} p_\infty^{\alpha(t_1)}(s_1) \prod_{n=1}^{N-1} \frac{p_\infty^{(\alpha(t_{n+1}))}(s_n)}{p_\infty^{(\alpha(t_n))}(s_n)} + O((\Delta t)^2) \\ &= \dots \\ &= \sum_{s_{N-1} \in \mathcal{S}} p_\infty^{\alpha(t_N)}(s_{N-1}) + N O((\Delta t)^2) \\ &= 1 + O(\Delta t). \end{aligned} \tag{C.10}$$

Then since $\log x \leq x - 1$, we have $\langle \log \hat{Q} \rangle \leq \langle \hat{Q} - 1 \rangle = O(\Delta t)$. But from (C.9) and (C.2), we have

$$\langle \log \hat{Q} \rangle = - \sum_{n=0}^{N-1} \langle \varphi^{(\alpha(t_{n+1}))}(\hat{s}(t_{n+1})) - \varphi^{(\alpha(t_n))}(\hat{s}(t_n)) \rangle$$

⁶⁶ $\text{Prob}[A|B] = \text{Prob}[A \text{ and } B] / \text{Prob}[B]$ is the conditional probability of an event A given that an event B is true.

$$\begin{aligned}
&= - \sum_{n=0}^{N-1} \langle \varphi^{(\alpha(t_{n+1}))}(s) - \varphi^{(\alpha(t_n))}(s) \rangle_{t_n} \\
&= - \sum_{n=0}^{N-1} \left\{ \Delta t \frac{d\alpha(t_n)}{dt} \left\langle \frac{d}{d\alpha} \varphi^{(\alpha)}(s) \right|_{\alpha=\alpha(t_n)} \right\rangle_{t_n} + O((\Delta t)^2) \right\}.
\end{aligned}
\tag{C.11}$$

By letting $N \rightarrow \infty$, we get the desired (C.5).

ACKNOWLEDGMENTS

It is a pleasure to thank Yoshi Oono for introducing us to the present subject and for various indispensable advices and suggestions. We wish to thank Kumiko Hayashi for related collaboration with one of us (Sasa), Hisao Hayakawa for valuable comments about boundary effects, Akira Yoshimori for useful discussions related to fluctuation-response relations, and Kyozi Kawasaki for valuable comments on the manuscript. We also wish to thank Ichiro Arakawa, Hiroshi Ezawa, Makoto Fushiki, Nobuyasu Ito, Christopher Jarzynski, Arisato Kawabata, Kim Hyeon-Deuk, Tohru Koma, Teruhisa Komatsu, Joel Lebowitz, Raphael Lefevre, Hiroshi Mano, Tsuyoshi Mizuguchi, Satoru Nasuno, Ooshida Takeshi, Kazuya Saito, Tomohiro Sasamoto, Masaki Sano, Ken Sekimoto, Akira Shimizu, Herbert Spohn, Masaru Sugiyama, and Hirofumi Wada for various useful discussions and comments during the years through which we have developed the present work.

The work of one of us (Sasa) was supported by grants from the Ministry of Education, Science, Sports and Culture of Japan, No. 16540337.

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